

APPLICATION OF HOLOGRAPHIC INTERFEROMETRY
TO THE INTERIOR BALLISTIC FLOW FIELD IN
THE BARREL OF A TWENTY MILLIMETER CANNON

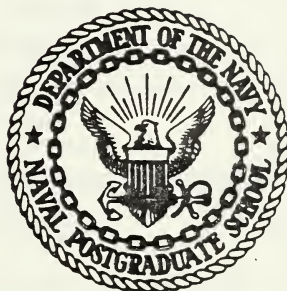
Richard Lewis Montgomery

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THESIS

APPLICATION OF HOLOGRAPHIC INTERFEROMETRY
TO THE INTERIOR BALLISTIC FLOW FIELD IN
THE BARREL OF A TWENTY MILLIMETER CANNON

by

Richard Lewis Montgomery

September 1976

Thesis Advisor:

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T175055

REPORT DOCUMENTATION PAGE

READ INSTRUCTIONS
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1. REPORT NUMBER	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) Application of Holographic Interferometry to the Interior Ballistic Flow Field in the Barrel of a Twenty Millimeter Cannon		5. TYPE OF REPORT & PERIOD COVERED Master's Thesis September 1976
7. AUTHOR(s) Richard Lewis Montgomery		6. PERFORMING ORG. REPORT NUMBER
9. PERFORMING ORGANIZATION NAME AND ADDRESS Naval Postgraduate School Monterey, California 93940		8. CONTRACT OR GRANT NUMBER(s)
11. CONTROLLING OFFICE NAME & ADDRESS Naval Postgraduate School Monterey, California 93940		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office) Naval Postgraduate School Monterey, California 93940		12. REPORT DATE September 1976
		13. NUMBER OF PAGES 99
		15. SECURITY CLASS. (of this report) Unclassified
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number)		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) The technique of holographic interferometry was applied to the study of gas core characteristics in the barrel of a 20mm cannon. Using standard hydrodynamic equations theoretical predictions were calculated. Holographic interferograms were made of the associated flow field near the projectile during firing. Reconstruction of the wavefront provided the necessary means of comparing experimental results with the theoretical values obtained.		

Application of Holographic Interferometry
to the Interior Ballistic Flow Field in
the Barrel of a Twenty Millimeter Cannon

by

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Lieutenant, United States Navy
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Submitted in partial fulfillment of the
requirements for the degree of

MASTER OF SCIENCE IN AERONAUTICAL ENGINEERING

from the
NAVAL POSTGRADUATE SCHOOL
September 1976

Thesis
M702
c.1

ABSTRACT

The technique of holographic interferometry was applied to the study of gas core characteristics in the barrel of a 20mm cannon. Using standard hydrodynamic equations theoretical predictions were calculated. Holographic interferograms were made of the associated flow field near the projectile during firing. Reconstruction of the wave-front provided the necessary means of comparing experimental results with the theoretical values obtained.

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LIST OF SYMBOLS

<u>SYMBOL</u>	<u>DEFINITION</u>
A	Cross-section area
C	Constant specifying thickness of shock region
E	Specific internal energy
j	Mass point number
M	Mass
P	Pressure
q	Artificial viscosity
t	Time
u	Velocity
V	Specific Volume
X	Eulerian Position
ρ	Density

ACKNOWLEDGMENT

The Author wishes to express his sincere appreciation to Dr. D. J. Collins for his invaluable guidance throughout the course of this study, and to the technical staff of the Department of Aeronautics, particularly P. Hickey and G. Middleton for their assistance in the construction and operation of the equipment used in this investigation.

This work was sponsored by the U. S. Naval Ordnance Station, Indian Head, Maryland, under Project Number 4-0029.

I. INTRODUCTION

For many years the field of theoretical interior ballistics was almost entirely confined to a single problem: given the characteristics of shot, charge, and gun, to calculate the muzzle velocity and peak pressure. (Ref. 1)

With the discovery of the laser and its application to holography, more interesting information can be obtained. It is possible to make a hologram of the projectile and its flow field, then reconstruct the image with exact detail.

Having a thorough knowledge of the physical characteristics of the internal gas flow field is essential in ballistic design. Although thermochemical constants for the products of combustion during actual gun firing are not well known, it is assumed that the gas and the solid grains move together as a homogeneous mixture. If this is true, then the conclusions of the Lagrange hypothesis are applicable to the interior ballistics of a gun.

The motion of the projectile creates a system of rarefaction waves in the breech, with relaxation occurring through the mechanisms of stress transfer in the bed and in the propellant gas. The dual wave system will accelerate the gas and the particles in the direction of the projectile

motion at the expense of stored internal energy. The more volatile gas will follow the projectile more readily than the particles. With progressive motion of the projectile, the initial unsteady flow may be expected to damp out and, as the motion evolves, to assume the quasi-equilibrium character of the Lagrange solution. This is a flow in which the mixture has uniform density, a linear velocity distribution and a quadratic pressure distribution. Eventually, the propellant is consumed entirely. Subsequent motion involves only the propulsion of the projectile by the reservoir of energetic gas. (Ref. 2)

It is the purpose of this investigation to utilize laser techniques and observe this flow field responsible for propelling the projectile as it transits through the barrel of a gun.

II. HOLOGRAPHIC INTERFEROMETRY

Holography is a process which is similar to photography in certain respects, but is nonetheless fundamentally different. Photography provides a method of recording the two-dimensional irradiance distribution of an image. Generally speaking each "scene" consists of a large number of reflecting or radiating points of light. The waves from each of these elementary points all contribute to a complete wave which we call the "object wave." This complex wave is transformed by the optical lens in such a way that it forms an image of the radiating object. It is this image which is recorded on the photographic emulsion.

Holography is quite different. With holography one actually records the object wave itself. This wave is recorded in such a way that subsequent illumination of the record serves to reconstruct the original object wave even in the absence of the object. A visual observation of this reconstructed wavefront then yields a view of the object or scene which is practically indiscernible from the original.

The method of recording the object wave is as follows. One starts with a single monochromatic beam of light which

has originated from a very small source. The requirement of coherence means that the light should be capable of displaying interference effects that are stable in time. This single beam of light is then split into two components, one of which is directed toward the object or scene; the other is directed to a suitable recording medium. The component beam that is directed to the object is scattered, or diffracted, by that object. This scattered wave constitutes the object wave, which now is directed to the recording medium. The wave that proceeds directly to the recording medium is the reference wave. Since the object and reference waves are mutually coherent, they will form a stable interference pattern when they meet on the recording medium. The detailed permanent record of this interference pattern on the recording medium is called the "hologram." This method is illustrated in Figure 1. When the hologram is illuminated with a beam of light which is similar to the original reference wave used to record the hologram, light will be transmitted only through the clear areas, resulting in a complex transmitted wave. Because of the recorded interference fringes, this wave conveniently divides into three separate components, one of which exactly duplicates the original object wave. By viewing

this reconstructed wavefront, one sees an exact replica of the original object. Three-dimensional images of opaque objects may be reconstructed and photographed from different viewing angles using a single hologram.

The above description of holography can be represented mathematically as follows:

$$\text{Let } \bar{E} = \bar{O} + \bar{R} \quad 2.1$$

Where \bar{O} represents the object or scene beam

\bar{R} represents the reference beam

$$\text{Then } E^2 = O^2 + R^2 + 2\langle \bar{O} \cdot \bar{R} \rangle \quad 2.2$$

Taking the time average:

$$\langle \bar{E}^2 \rangle = I = I_O + I_R + 2\langle \bar{O} \cdot \bar{R} \rangle \quad 2.3$$

The term $2\langle \bar{O} \cdot \bar{R} \rangle$ in equation 2.3 is the interference term. Without interference the intensity of the two beams are merely additive. With the utilization of monochromatic light derived from a single ideal source, interference is always possible.

Uncorrelated light beams, as from two different light sources, are uncorrelated and are called incoherent. Coherent radiation produces interference effects. The superposition of incoherent radiation yields the addition of the intensities of the object and reference beams.

The interference term contains both amplitude and phase information. Consider two waves such that:

$$\bar{O} \cdot \bar{R} = \frac{1}{2}(\bar{O}e^{-i\omega t} + \bar{O}^*e^{i\omega t}) (\bar{R}e^{-i\omega t} + \bar{R}^*e^{i\omega t}) \quad 2.4$$

Then

$$\bar{O} \cdot \bar{R} = \frac{1}{2} \left\{ \bar{O} \cdot \bar{R} e^{-2i\omega t} + \bar{O}^* \bar{R}^* e^{2i\omega t} + \bar{O} \cdot \bar{R}^* + \bar{O}^* \cdot \bar{R} \right\} \quad 2.5$$

$$2 \langle \bar{O} \cdot \bar{R} \rangle = \frac{1}{2} (\bar{O} \cdot \bar{R}^* + \bar{O}^* \cdot \bar{R}) \quad 2.6$$

If $O_1 = O_1 e^{ig_1}$ etc. and $R_1 = r_1 e^{ih_1}$

$$\begin{aligned} 2 \langle \bar{O}_1 \cdot \bar{R}_2 \rangle &= O_1 r_1 \cos(g_1 - h_1) + O_2 r_2 \cos(g_2 - h_2) \\ &+ O_3 r_3 \cos(g_3 - h_3) \end{aligned} \quad 2.7$$

Thus the interference term contains both amplitude and phase information. From equation 2.6 it is evident that interference occurs only when light beams of the same polarity interact with one another.

The complete interference equation is:

$$I = \langle \bar{E}^2 \rangle + I_R + I_O + R \cdot O^* + O \cdot R^* \quad 2.8$$

where $\langle R \cdot R^* \rangle = I_R$

and $\langle O \cdot O^* \rangle = I_O$

The reconstruction process can also be described with equation 2.8. The amplitude transmittance of the hologram

is assumed to be proportional to the intensity

$$t(x) + KI \quad 2.9$$

On reconstruction with the reference beam R , the following is obtained:

$$R \cdot KI = R(I_R + I_O) + R \cdot R \cdot O^* + R \cdot R^* \cdot O \quad 2.10$$

The last term in equation 2.10 is the reconstructed object beam.

A primary consideration in the technique of holographic interferometry of flow fields is the source of coherent light. The Q-switched ruby laser has proved to be an excellent light source for these applications. It provides the high power necessary to expose the plate in a time frame suitable for freezing the motion of the flow field.

The wavelength of this laser is $6943 \overset{0}{\text{\AA}}$, which is compatible with AGFA-GEVAERT 10E75 holographic film plates. (Ref. 3)

III. EXPERIMENTAL LAYOUT

A. GENERAL PHYSICAL ARRANGEMENT

The experiment was conducted at the Naval Postgraduate School Rocket Laboratory. The laboratory contained four test cells measuring 12' X 17' with reinforced concrete walls 12" thick. A control room with observation windows was located directly behind the test cells.

The 20mm cannon was mounted horizontally on a rocket test stand. Two steel mounts were used to secure the barrel in place at a height of 6.5 inches from barrel center line to the top of the test stand.

Two large wooden tables were constructed and placed parallel to and on either side of the test stand. The tables provided a platform for the optical equipment necessary to obtain holograms. The tables were rigidly fastened together; however, they were completely isolated from the test stand to ensure stability during cannon operation. Furthermore, plywood boxes were constructed to fit over the tables and completely house the optical equipment. The plywood boxes not only acted as protection for the equipment but also acted as a light shield for the

holographic process. The tops of the plywood boxes were hinged in order to allow easy access to the optical equipment.

The muzzle of the cannon faced a bullet trap located 13 feet outside the test cell. The bullet trap contained an 18" X 18" X 1½" armored plate, tilted 45° from the path of the projectile, and a sand trap measuring 5' X 5' X 2½'.

Upon bullet impact, the plate shattered the projectile and deflected the fragments into the sandtrap. In order to provide additional safety, the entire sandtrap was housed inside a steel turret for a 5" gun mount measuring approximately 15' X 20' X 10'.

An electrical firing mechanism was placed at the breech end of the cannon. The firing sequence was directed from the control room.

A light shield was provided to cover the observation window during placement and removal of the holographic plates.

The ruby laser and its components were fixed in position in a test cell adjacent to the cell housing the 20mm cannon. The purpose of this placement was necessary not only for space consideration but mostly for protection of the instrument. A specially constructed table provided support for the laser rail system. The laser was placed normal to the

wall separating the two cells. (Figure 2) A 2-inch hole was drilled through the concrete wall to allow beam passage. A water source for the laser head and output etalon cooling system was incorporated within the test cell. The laser was equipped with a remote control making it possible to fire either from the test cell or the control room. (See Figure 3)

B. BARREL INSTRUMENTATION

For viewing the projectile inside the cannon a .817" diameter hole was drilled completely through the barrel 4.5" from the muzzle. In order to preserve the integrity of the barrel, projectile and flow field, plexiglass windows were designed to seal the port and provide observation inside the barrel. (See Figure 4)

The windows were milled from optical quality 3/4" plexiglass. Two windows were pressure tested in a simulated barrel to 6000 PSI, thus ensuring strength capabilities necessary to withstand internal pressures present. (See Figure 5)

Figure 6 shows the design consideration met for mounting the windows in the barrel. Figure 7 shows the actual barrel with window and with collar.

Figure 8 shows the collar device used to secure the windows in the barrel.

A Kistler 607A pressure transducer was installed 5.5 inches from the breech end of the barrel. This location was just ahead of the tip of the projectile prior to firing. The signal from the transducer was relayed to a Kistler model 504 universal charge amplifier located in the control room. The signal from the charge amplifier was passed to a Textronix 549 storage oscilloscope. The oscilloscope allowed the signal to be time delayed by a predetermined amount and then amplified to +30 volts, which in turn was used to trigger the xenon flash tube of the Korad K-1 pulsed ruby laser.

A Kistler 603H pressure transducer was located 2.5 inches aft of the observation ports. The signal from the transducer was relayed to a Kistler model 504A universal charge amplifier located in the control room. The signal from the charge amplifier was passed to a Hewlett Packard Model 214A pulse generator where it could be delayed and amplified. The resulting pulse was used to energize the Pockel cells of the Korad K-1 pulsed ruby laser.

The muzzle velocity was measured by the use of two Oehler Model 55 ballistic velocity screens. The screens

were mounted 4 feet apart and placed 81.25 inches from the muzzle of the cannon. As the projectile passed through each screen a 12-volt pulse with an adjustable 2-8 milli-second pulse length was produced and relayed to an Oehler Model 21 chronograph. The two pulses provided a start and stop for the chronograph. Tables of velocities were provided for known screen separation. (See Figure 9)

C. OPTICAL SYSTEM

Figure 10 shows the optical layout used to accomplish the holography. The Korad K-1 pulsed ruby laser was used for the holography process. By utilizing the laser system in the Q-switch mode of operation, high power single transverse mode output could be obtained. A Pockel cell was used to achieve the Q-spoiling required for peak output power.

When operating the Korad K-1 pulse ruby laser in the tem_{00} mode a peak power of 2.5 megawatts with pulse energy of .050 joules over a pulse width of 20 nanoseconds can be realized. The output beam measured approximately 2mm in diameter at a wavelength of $6943\overset{\circ}{\text{A}}$ with a coherence length that exceeds one meter. Figure 3 shows a photographic view of the laser installation.

The laser beam passes through a 2-inch hole in the concrete wall then through another 2-inch hole in the plywood boxes where it first contacts a narrow-band filter which removes the undesired light from the xenon flash tube. The beam then strikes a 2-inch round beam splitter where it is divided into two wave fronts, a scene beam and a reference beam. The intensity of the reference beam is about twice that of the scene beam.

The scene beam is directed along the centerline of a 2.5 meter optical bench where prior to striking mirror #1 it passes through a collimating lens, double concave lens and another collimating lens.

The lens arrangement was designed to allow the scene beam to be expanded to a diameter compatible with the hole drilled through the barrel of the 20mm cannon.

Mirror #1 directed the beam through the windows in the 20mm cannon and onto mirror #2. In order to accomplish this, 3-inch holes were cut in the plywood boxes to permit the beam to pass, allowing enough tolerance for adjustment to ensure that the beam passed through the windows normal to the cannon's axes. Furthermore, mirror #1 was secured to a gimbal mount which allowed a fine adjustment to be made in the horizontal and vertical axes.

Mirror #2 directed the scene beam down the centerline of a 1.5 meter optical bench where a second narrow-band filter was located to remove the unwanted flash from the cannon blast. The beam then proceeds through an expanding collimating lens to mirror #3 where it is directed to the holographic plate. The location of the expanding collimating lens makes it possible to enlarge the scene beam from test section (window size) diameter to a diameter of approximately 4-inches.

After passing the beam splitter the reference beam proceeded to mirror #4 on a 2.0 meter optical bench. The physical arrangement allowed the reference beam to be adjusted to the same length as the scene beam. Mirror #5 directs the beam through two series of expanding--collimating lenses which enlarged the reference beam to approximately 4-inches in diameter at the holographic plate.

Throughout the entire system the optical benches were bolted to the tables on specially designed cross feet which allowed the system to be leveled by adjustment knobs located at each crossfoot. The alignment procedure was greatly simplified by the use of mirrors which contained screw type adjustments for vernier-scale movement about the horizontal and vertical axes. In addition, all the optical components

could be easily positioned along the optical bench. Figure 11 shows the actual optical layout with one plywood box removed to show the arrangement.

The alignment of the system was accomplished by the use of a coherent radiation 3-milliwatt helium-neon continuous wave laser. This laser was mounted on a stand which was placed perpendicular to the axis of the ruby laser cavity. By firing the ruby laser on an exposed polaroid paper a "spot" could be obtained which was used in the alignment process. By placing a mirror at a 45° angle in the ruby laser cavity, the CW beam could be directed through the cavity and centered on the "spot." This centered beam would then coincide with the ruby laser beam and the optical system could be accurately aligned.

IV. FIRING SEQUENCE

All the electrical equipment was turned on to allow the required warm-up time while the test section and optical system were being prepared and aligned. The barrel test section assembly required particular care when installing the plexiglass windows, to ensure that the faces were parallel to the center line of the cannon and normal to the laser beam's path.

After the system was aligned, all electrical equipment was checked for proper settings and all timers zeroed. The opening into the plywood box containing the holographic plate was covered and the alignment mirror removed. The test cell was closed and a holographic plate was placed in its holder. The test cell door was raised to a level just above the muzzle of the 20mm cannon. At this time the cannon was loaded.

The individual who was loading the cannon and connecting the firing mechanism carried with him a safety key which broke the firing circuit at the control panel to prevent accidental firing prior to his clearing the test area. Following loading, the opening into the plywood box

containing the hologram was uncovered and control was then commenced from the control room. All electrical equipment was scanned and the warning horn sounded to alert personnel of the impending shot. The firing sequence was then initiated. A schematic of this sequence is shown in Figure 12.

The charge switch for the laser capacitor was activated. While the capacitor bank was charging, the safety key was installed in the fire control panel and power supplied to the firing mechanism. When the laser ready light illuminated the firing mechanism, capacitors were charged and the cannon fired. Figure 13 shows a view of the control room and monitoring equipment.

The firing process was observed through the observation window. A light shield was placed against the window after firing to protect the hologram from unwanted illumination.

Actual bullet movement was used to fire the laser. On initial firing, a pulse from the Kistler transducer located at the breech was passed to the Textronix 549 storage oscilloscope, where it was delayed and amplified, then used to trigger the xenon flash tube of the Korad K-1 pulsed ruby laser. Considering that the pumping time for the laser is approximately 1000 microseconds and that

approximately 1500 microseconds are needed for projectile travel to the test area, 500 microseconds was used for the pulse delay.

When the projectile reached the second Kistler transducer another pulse was initiated that was relayed to a Kistler model 504A charge amplifier then to a Hewlett Packard Model 214A pulse generator. The pulse generator provided the voltage necessary to trigger the Pockel cell of the Korad K-1 pulsed ruby laser. This unit allowed for a variable signal delay which was used to adjust the time interval for laser firing. Two Monsanto Model 101B timers were incorporated into the system at various locations to provide checks on intervals of interest. Also a Korad KD energy monitor was employed to check the actual laser firing interval.

After firing, the test cell was closed and the hologram removed for processing. The armor plate was inspected for integrity and repositioned if necessary. The 20mm cannon was unloaded and the windows removed and examined for damage.

V. HOLOGRAPHIC FILM AND PROCESSING TECHNIQUE

The Korad K-1 pulsed ruby laser delivered a beam at a wavelength of $6943\overset{\circ}{\text{A}}$. In order to minimize the effects of extraneous light leakage into the system a photographic emulsion with narrow band sensitivity centered in this region was selected. Agfa-Gevaert 10E75 holographic plates were found to be the most suitable for this purpose. This film has a resolution capability of 2800 lines per mm. For holograms produced with $6943\overset{\circ}{\text{A}}$ light this is nearly the required maximum resolution. Reference 4 gives a spectral sensitivity curve for the emulsion.

Following exposure to the laser light the hologram plate was removed from its holder and placed in a closed container and taken to a dark room for development. The initial processing required a five minute bath in kodak D-19 developer. The entire five minute bath was completed in total darkness. Then the plate was rinsed and placed for five minutes in a standard fixer. After 30 seconds in the fixer it was permissible, although not necessary, to turn on green photographic lights in the dark room. From the fixer the plate was washed in water for five minutes and then allowed to air dry. During the entire development

procedure, when it became necessary to touch the hologram it was handled by the edges in an attempt to keep the hologram clear of unwanted finger markings.

When using the 20-nanosecond ruby pulse, it was not possible to control exposure time. Therefore, to ensure the desired intensity, a combination of suitable neutral density filters were placed in the beam paths.

VI. RECONSTRUCTION

To reconstruct the holograms a 15-milliwatt Spectra Physics continuous wave, helium-neon laser was used for the reconstructing wave. A Spectra Physics collimator was fastened to the laser, causing the beam to be expanded to approximately four inches in diameter. The beam was directed to pass through the hologram as outlined in Part I. The converging real image was then photographed with a single reflex polaroid camera using type 55 positive-negative film. This film has a resolution capability of 150-165 lines per mm negative, 14-17 lines per mm positive, thus providing excellent results. The reconstruction process is illustrated in Figure 14. The negatives were further processed at the Naval Postgraduate School photo lab, from which prints were produced.

VII. COMPUTER PROGRAM FOR PREDICTIONS OF FLOW PARAMETERS

The computer program used to predict the velocity of the projectile, pressure and total energy of the flow field was an adaption of a program developed at the Naval Ordnance Laboratory. The program was originally concerned with the analysis of hypervelocity model launchers (Ref. 5). The method of analysis used was essentially a one-dimensional, Lagrangian scheme where the field was divided into six regions each of which in turn was divided into zones. At the interface of each zone mass points were inserted. Each mass was considered to consist of one-half of the mass of the adjacent zone. The hydrodynamic equations, in finite difference form, were then applied to each mass point during the particular interval of interest. The method employed was the "q" method of Von-Neumann and Richtmyer (Ref. 6 and 7).

The following equations were used for this method:

Isentropic flow energy equation;

$$\frac{\partial E}{\partial t} = -(P+q) \frac{\partial v}{\partial t}$$

Equation of motion;

$$\frac{\partial u}{\partial t} = - \frac{\partial (P+q)}{\partial x} \frac{1}{M} A(x)$$

Equation of state;

$$P = P(E, v)$$

$$M = \int^X (X)A(X)dx$$

$$\text{with } \begin{cases} \frac{C_o^2}{v} \frac{\partial u}{\partial y} & , \frac{\partial u}{\partial y} < 0 \\ 0 & , \frac{\partial u}{\partial y} \geq 0 \end{cases}$$

The artificial viscosity term "q" was added to the pressure term in the energy and motion equations in order to spread variable changes created by the shock over a finite region. This allows the equation variables to be considered continuous across the shock. The constant C_o permits adjustment of the shock "thickness."

The equations were written in finite difference form with initial values of E_o , P_o , and V_o being provided for each region. In order to maintain stability during the process, a new time increment was calculated for each cycle.

During each cycle the pressure was calculated at each mass point using the equation of state and energy. The differential in pressure between mass points was then applied to the equation of motion to determine the acceleration and velocity of each mass point.

For each region it is necessary to input the initial temperature, pressure, molecular weight and a geometrical description.

The program was written in FORTRAN. A listing of the program and the input is given in Appendix A.

VIII. HOLOGRAPHIC RESULTS

Initially the first few holograms obtained appeared to be in the region several centimeters in front of the projectile. However, when further experimental studies did not give the desired results, an investigation was initiated to examine the laser system. It was then discovered that a short circuit had occurred between the plate and cathode of the large thyatron of the Korad power supply. This short circuit would occur approximately 8 minutes following the application of power. This malfunction caused a firing pulse to be continually delivered to the Pockel cell; thus, nearly two-thirds of the seventy-five test firings resulted in holograms in which the laser had fired from 50 to 200 microseconds early. To further compound the problem the Korad KD energy monitor was not available to confirm actual laser firing.

With the incorporation of the energy monitor into the system, and careful monitoring of the power supply, several good holograms were obtained. Figure 15 shows a series of compression waves approximately 2 cm in front of the projectile. Figure 16 shows these same type of waves

approximately 1 cm in front of the projectile. A traveling bow wave can be seen in Figure 17. It is believed that this wave is approximately 3 mm in front of the projectile.

Due to time consideration allowed for this study, the area just behind the projectile was not captured; however, Figure 18 shows a hologram obtained approximately 30 microseconds following projectile passage through the test area. The effects of powder blast not only etch the plexiglass windows but also leave a carbon deposit over the inner faces, resulting in a clouded view of the test area. Further investigations will determine if this powder blast is directly behind the projectile or if there are several microseconds delay between the gas particles and the projectile.

IX. COMPARISON OF ANALYTICAL AND EXPERIMENTAL RESULTS

Analytical results were obtained previously by Robert G. Bettinger (Reference 8) during his work concerning gas core characteristics in the muzzle environment of the 20mm cannon.

Figures 19 and 20 are outputs obtained by Bettinger. Figure 19 summarizes the major input data and initial conditions required, and demonstrates the output format used for representing these data. As shown in Figure 19, a printout was obtained every 0.2 milliseconds. Figure 20 illustrates the output obtained just as the projectile exits the barrel; at this time a muzzle velocity of 1064 meters per second was obtained.

It must be emphasized that the program (Reference 5) does not take into consideration the effects of frictional forces on the projectile. Therefore, in order to obtain a more realistic solution either the program must be modified or the powder parameters altered to account for this constraint. Figures 19 and 20 resulted from the latter choice.

In order to verify these results it was necessary to analyze the powder used to propel the 20mm projectile.

The type powder used in the 20mm cartridge was WC870 with a charge weight of 590 grains. WC870 is a sphere of .305" average grain diameter, with a specific gravity of 1.56 grams/cc. A representative composite is:

Nitrocellulose (13.15%N)	=	81.49%
Nitroglycerine	=	10.0 %
Dibutylphthalate	=	5.5 %
Diphenylamine	=	1.0 %
CaCO ₃	=	0.1 %
AsH	=	0.5 %
Graphite	=	0.15%
Na ₂ SO ₄	=	0.16%
K ₂ SO ₄	=	0.75%
SN ₂ O ₂	=	0.75%
Ethyl Acetate	=	0.10%
H ₂ O	=	0.80%

The percentages are given of the dry weight, so that the sum of the ingredients up to the last two constituents is 100%.

The average thermochemical properties of this composition are (by Hirschfelder's approximation, reference 1) as follows:

T ₀	=	2856°K
n	=	0.04218 grams/mol
γ	=	1.2394
F	=	335068 ft-lbs/md
b	=	0.943 cc/gram

The molecular weight of the constituents can be found directly except for nitrocellulose. The nitrocellulose in propellant compositions varies in its nitrogen content. The cellulose molecule is a large one but, for present

purposes, it can be written $C_6H_7O_2(OH)_3$. On nitration, $X(OH)$ groups are replaced by (ONO_2) groups, the value of X depending on the nitrogen content. The resulting compound is $C_6H_7O_2(OH)_{3-X}(ONO_2)_X$. The molecular weight is easily found to be $(162.14 + 45X)$ and, if Y is the percentage nitrogen content, $Y = \frac{1400.8X}{162.14 + 45X}$. This gives $X = \frac{162.14Y}{1400.8 - 45Y}$. Thus for a given nitrogen content Y and X can be calculated and the atomic composition found from:

$$C = \frac{6}{162.14 + 45X} \quad H = \frac{10 - X}{162.14 + 45X} \quad N = \frac{Y}{1400.8} \quad O = \frac{5 + 2X}{162.14 + 45X}$$

The heats of formation of the solid propellant can be calculated as outlined in Reference 10.

Inputting the exact values into the computer program resulted in a value of approximately 1463 M/sec. Assuming a projectile drag coefficient of 0.28 (Reference 9), this gives a muzzle velocity of 1036 meters per second which is in excellent agreement with Bettinger's theoretical results.

Furthermore, the maximum possible muzzle velocity (Reference 1) may be calculated from the following:

$$V_m = \frac{2}{\gamma - 1} (RT_0)^{\frac{1}{2}}$$

Using this equation a value of 1097 meters per second is

obtained. The projectile velocity was measured during each firing, and a range of 1020 to 1060 meters per second was obtained.

These values are in excellent agreement with the computer program.

X. SUMMARY AND RECOMMENDATIONS

A considerable amount of difficulty was experienced while attempting to capture the projectile in the test area. Considering the velocity and length of the projectile, passage through the test area occurs within approximately 80 microseconds. Furthermore, considering just the base of the projectile, a time interval of approximately 20 microseconds would result in complete passage of the base of the projectile through the test area. Thus, timing of the laser firing with projectile firing is indeed quite critical.

Referring to Figure 21, it can be seen that the velocity of the projectile approaches a constant value at a distance of approximately 90 cm from the breech of the barrel. It was this fact that prompted the barrel modification to incorporate the pressure transducer near the test area as outlined in Part III Section B. By controlling the firing of the Pockel cell with this transducer, more consistent results were expected.

Theoretically, if the pressure transducer responded instantaneously to the passage of the gas ring of the projectile, the signal produced could be used to pulse the

Pockel cell of the laser just as the nose of the projectile entered the test area.

Unfortunately, 0.5 volts was required to trigger the Hewlett Packard Model 214A pulse generator, while the Monsanto timers responded immediately to projectile passage. Referring to the pressure trace obtained from the pressure transducer (Figure 22), approximately 100 microseconds could pass before the required 0.5 volts was obtained.

In an attempt to confirm the actual passage of the projectile through the test area the pressure transducer was replaced by a temporary contact switch. This switch could only be triggered by actual contact with the gas ring of the projectile. The test confirmed the correct timing of the projectile, agreeing with the results obtained with the pressure transducer as far as the Monsanto timers were concerned.

Due to the fact that most pulse generators require at least 0.5 volts input as a trigger and that the pressure transducer used takes anywhere from 0-100 microseconds to reach 0.5 volts, it is felt that a more positive device must be used to sense the actual position of the projectile. This could be accomplished with a contact switch designed specifically for this purpose.

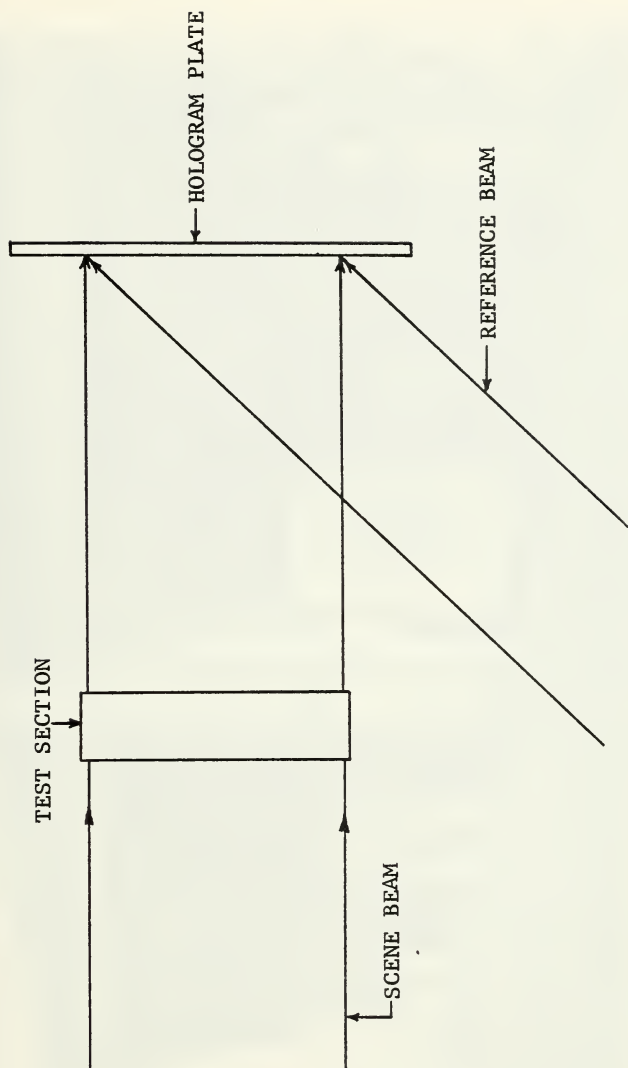
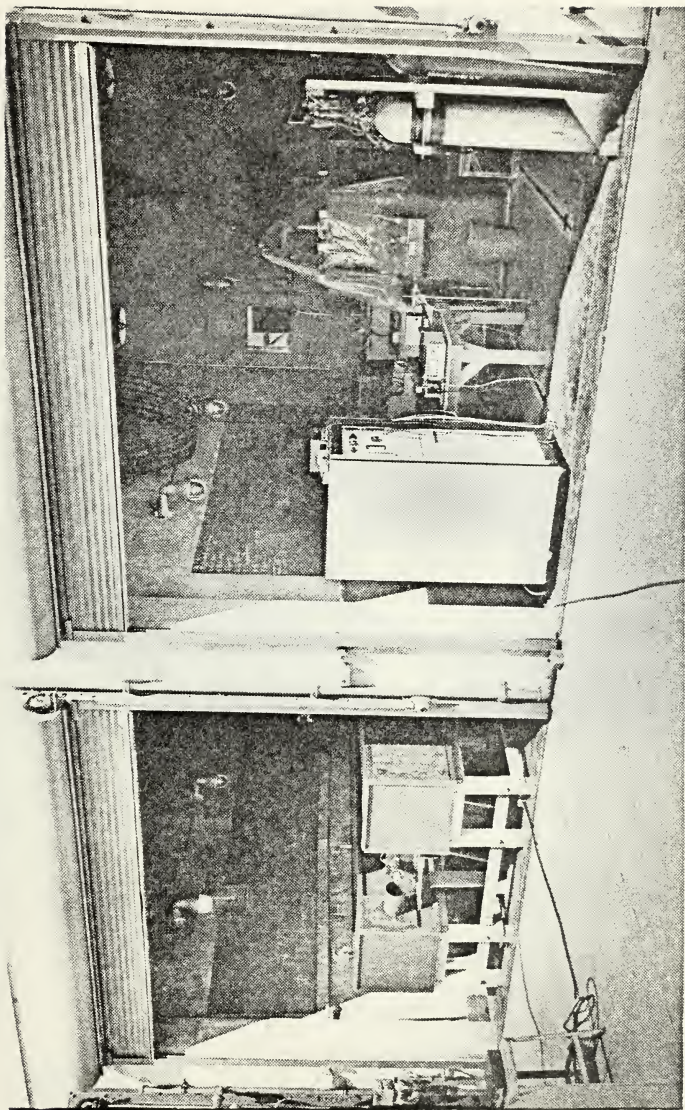


Figure 1. Direct Illumination Method of Obtaining a Hologram



Cannon and Optics Cell

Laser Installation

Figure 2

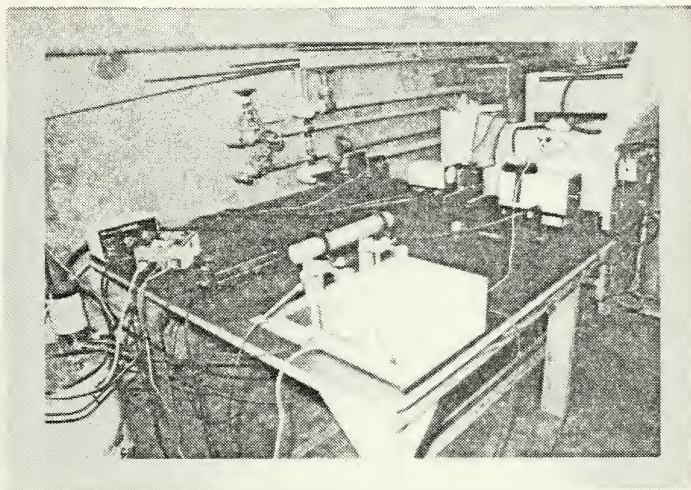


Figure 3. Laser Setup

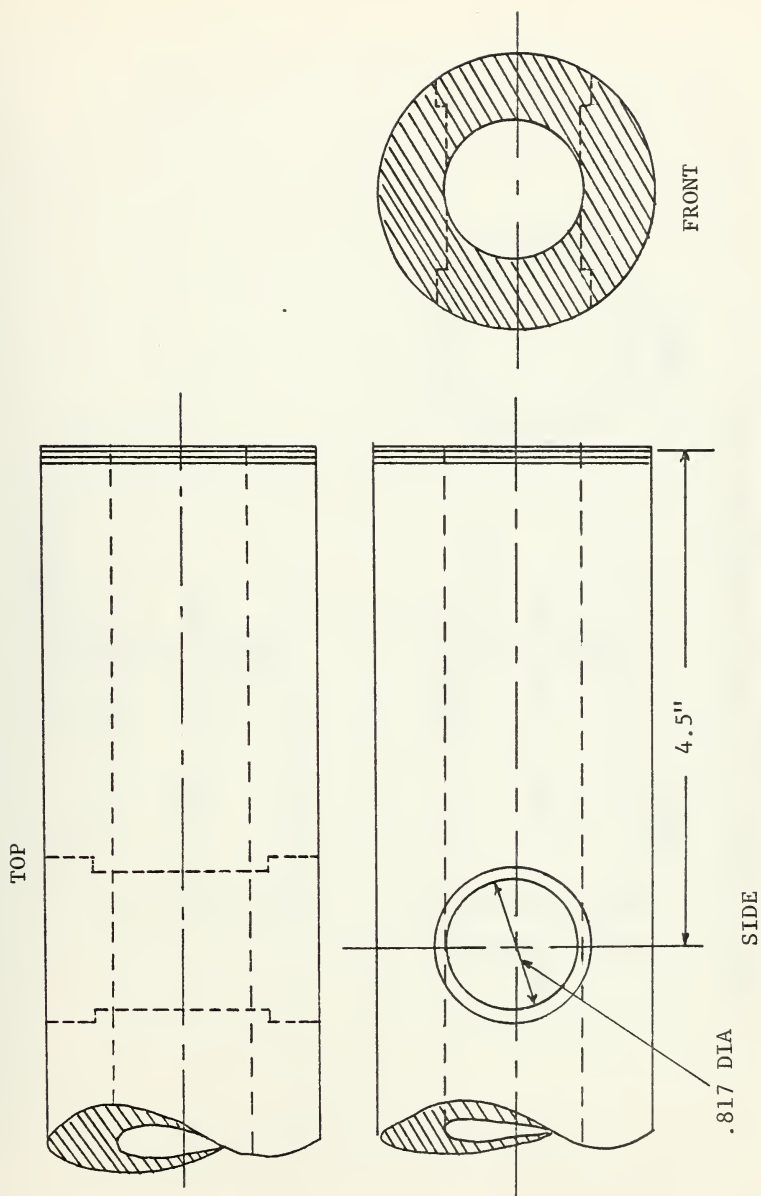
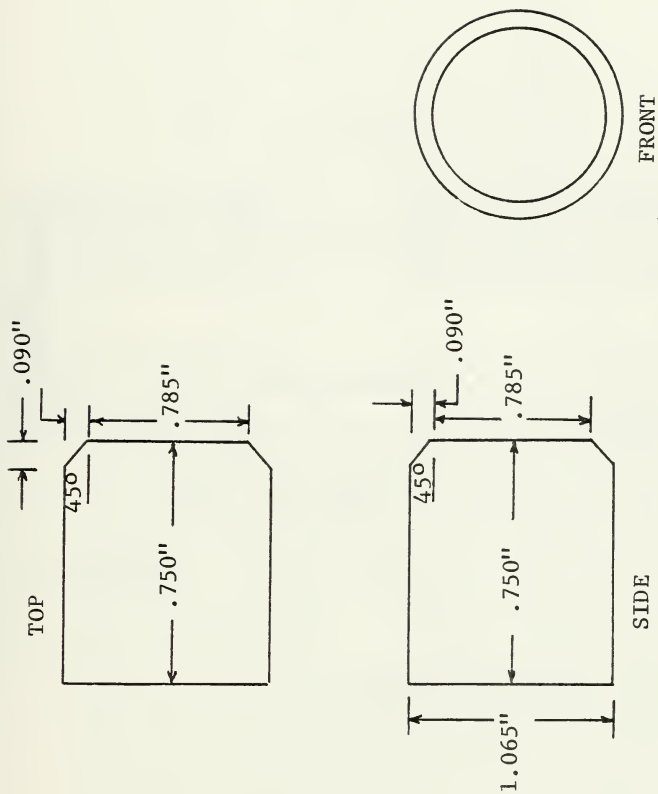


Figure 4. Barrel Design



NOTE: Windows to be seated with #118 O-ring

Figure 5. Plexiglass Windows

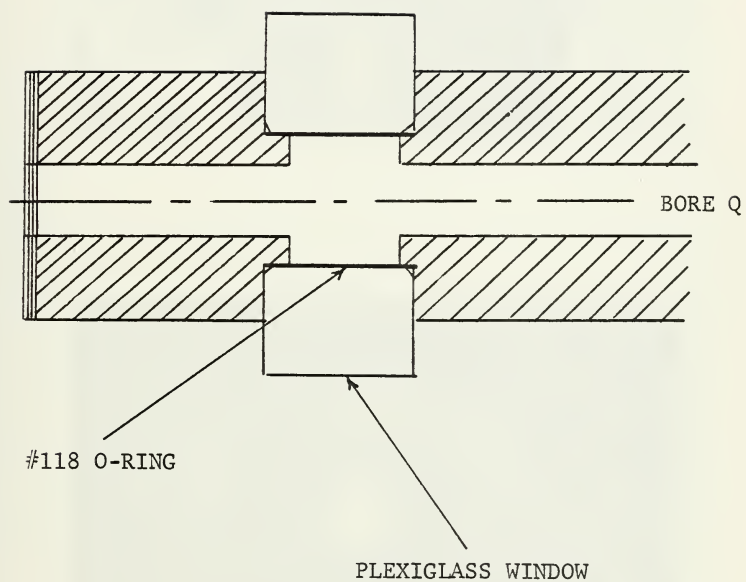


Figure 6.
Top Cutaway View of Barrel with
Plexiglass Window Installation

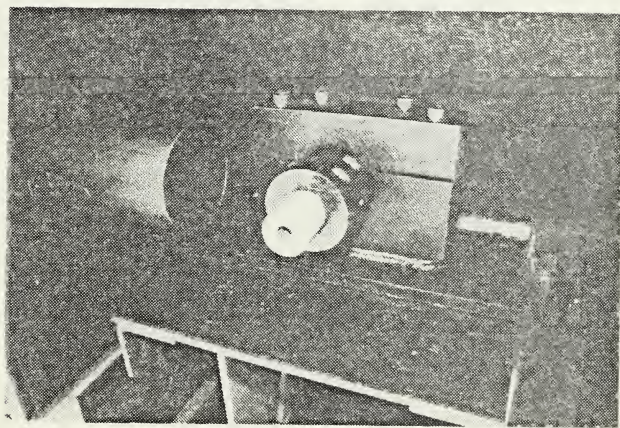
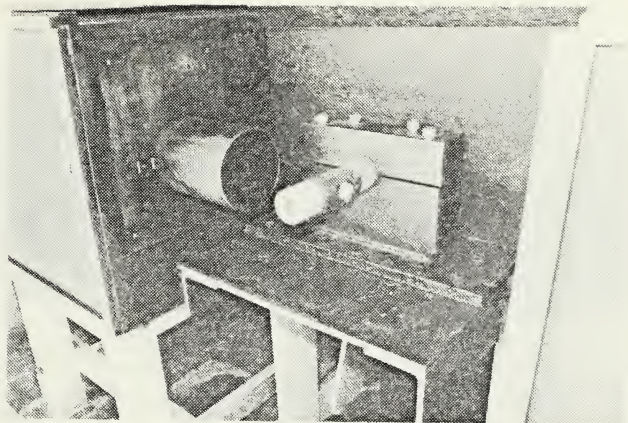


Figure 7. Barrel with Windows and with Collar

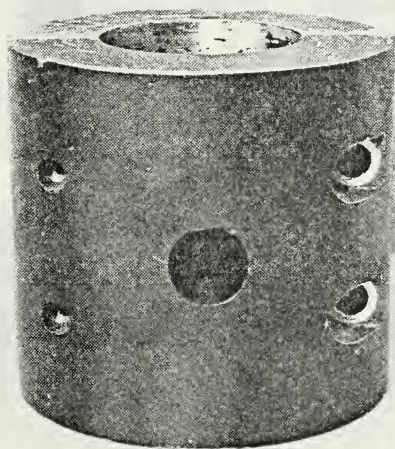
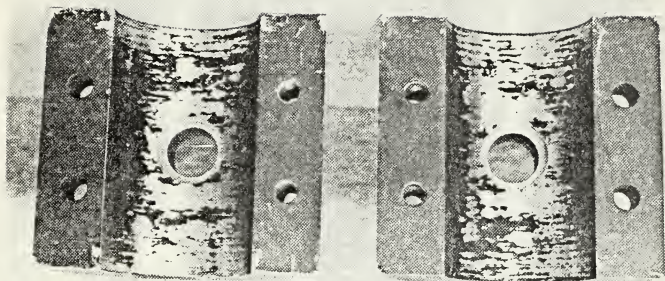


Figure 8. Collar Device

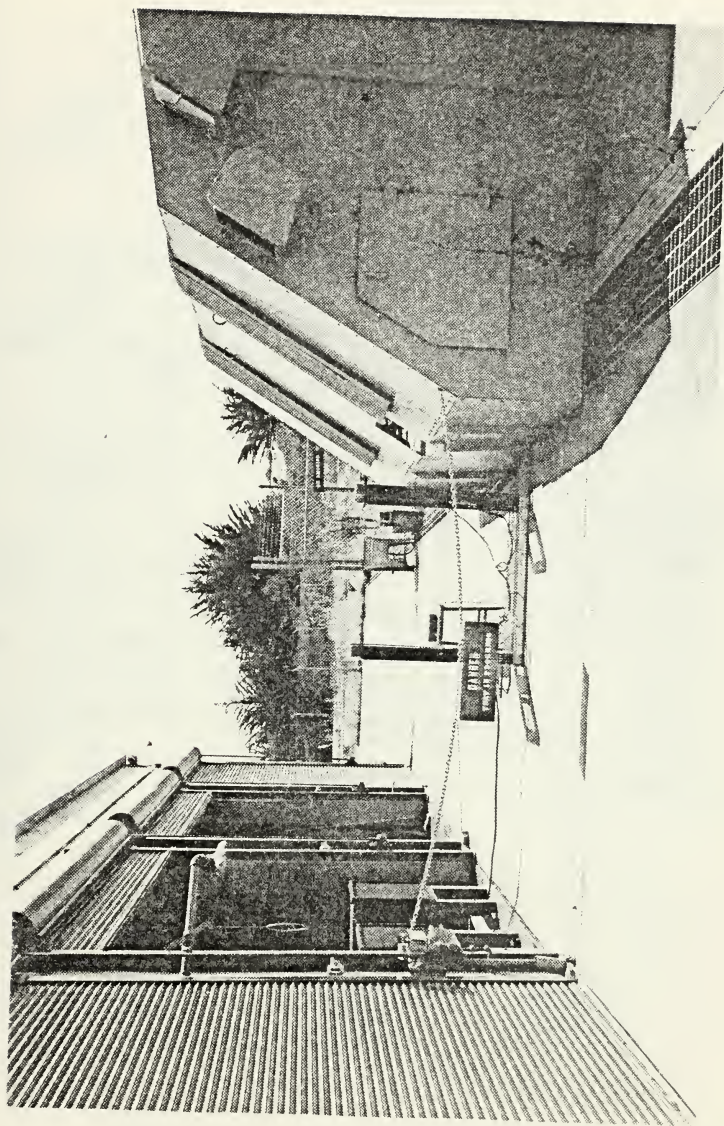


Figure 9. Projectile Path and Turret with Velocity Screen in Place

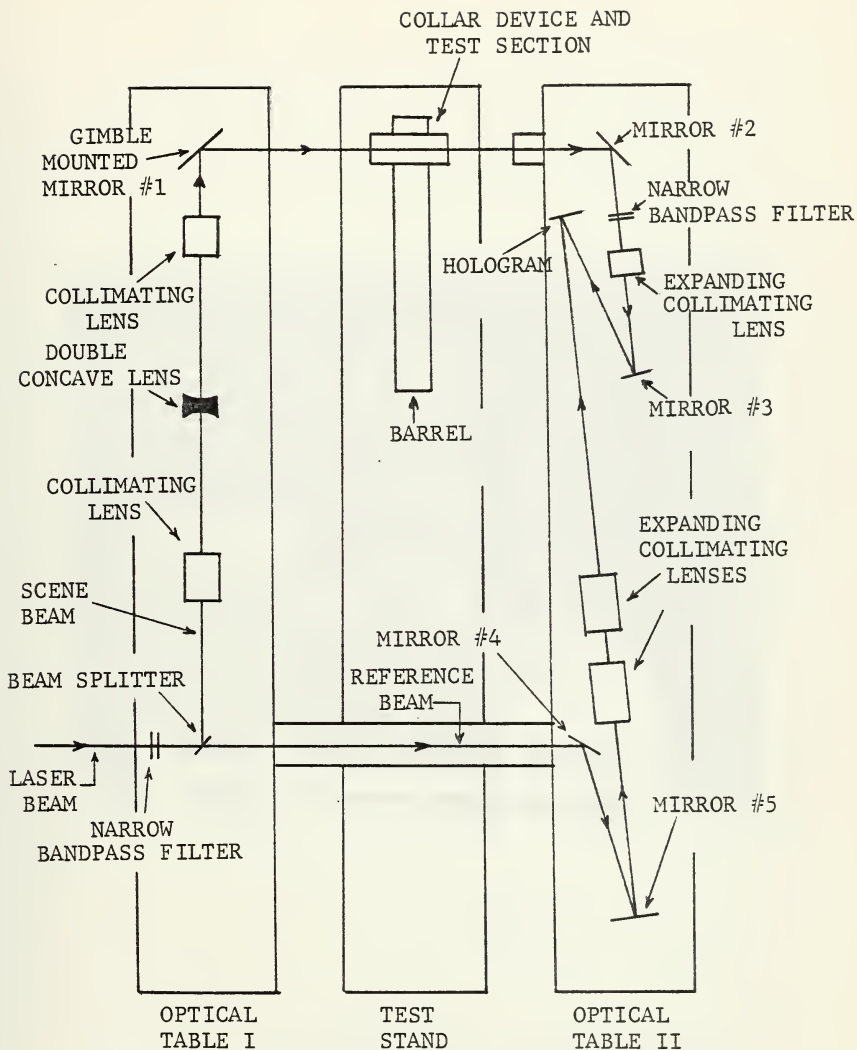


Figure 10. Optical Arrangement

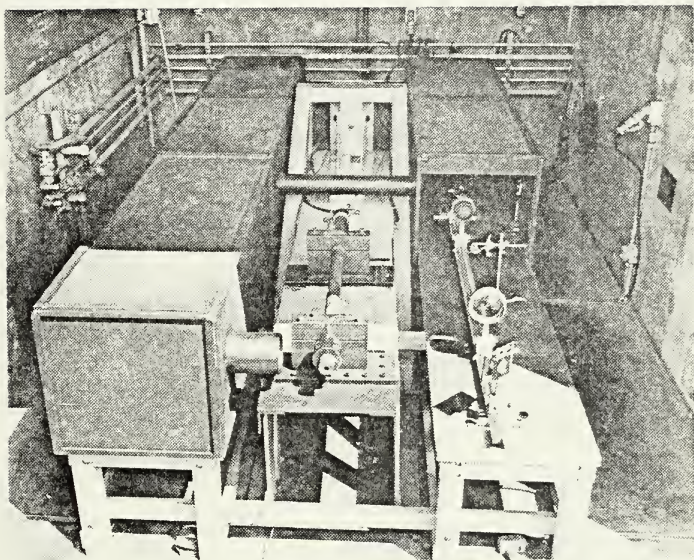


Figure 11. 20mm Cannon with Optical Platform

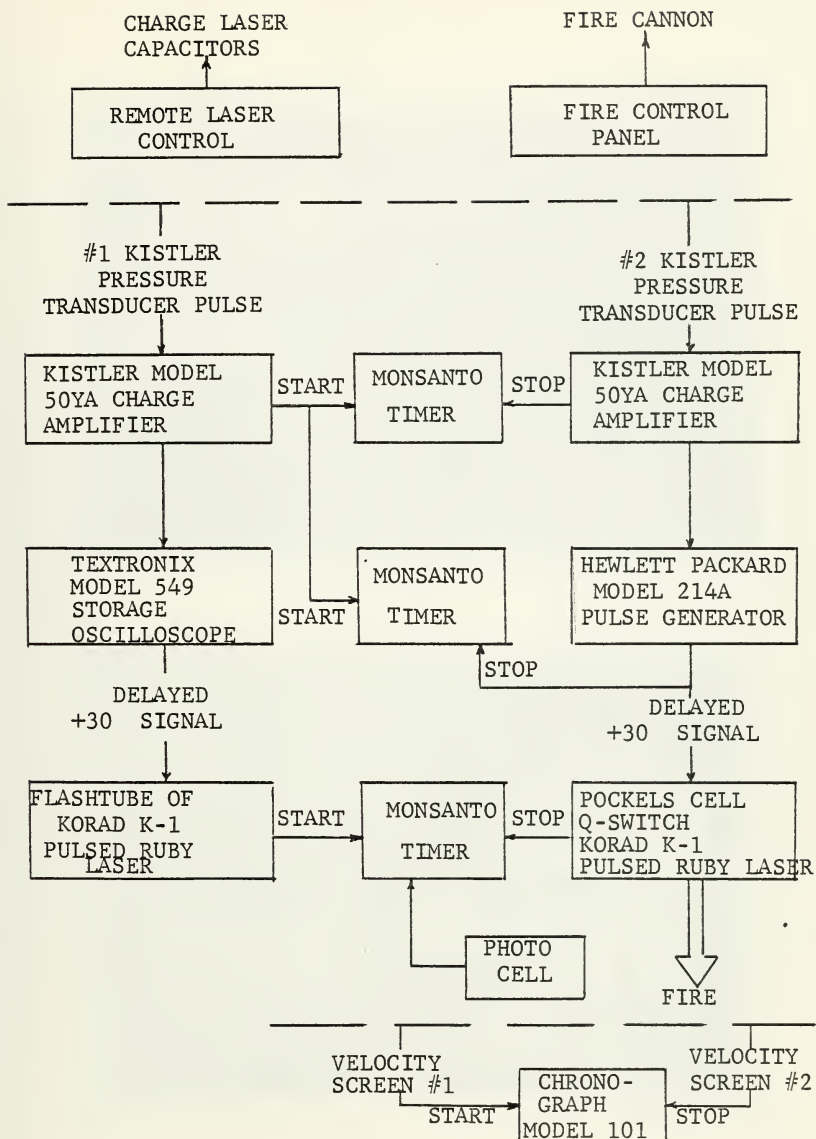


Figure 12. Firing Sequence

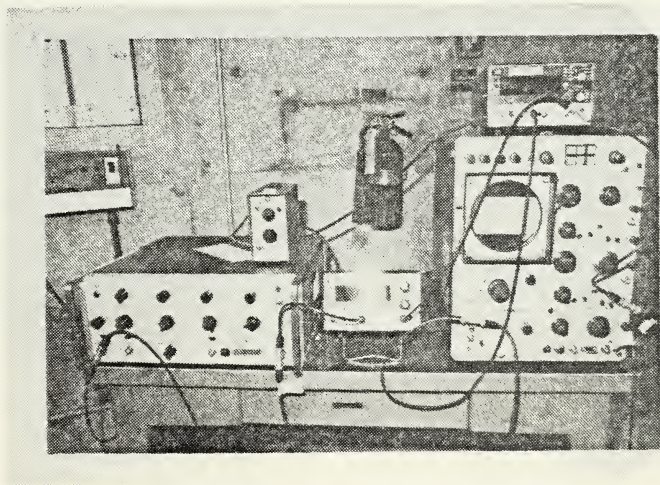
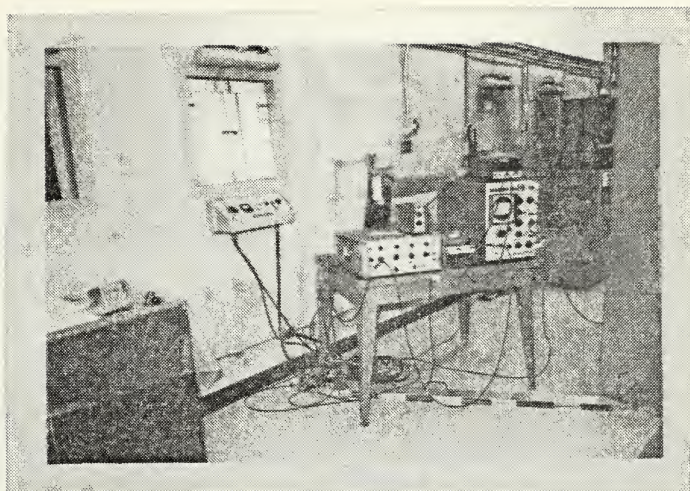


Figure 13. Control Room and Monitoring Equipment

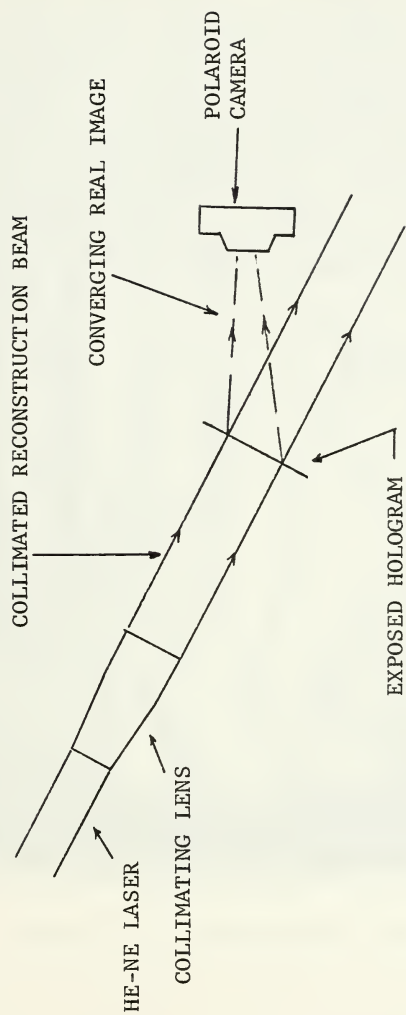


Figure 14. Reconstruction

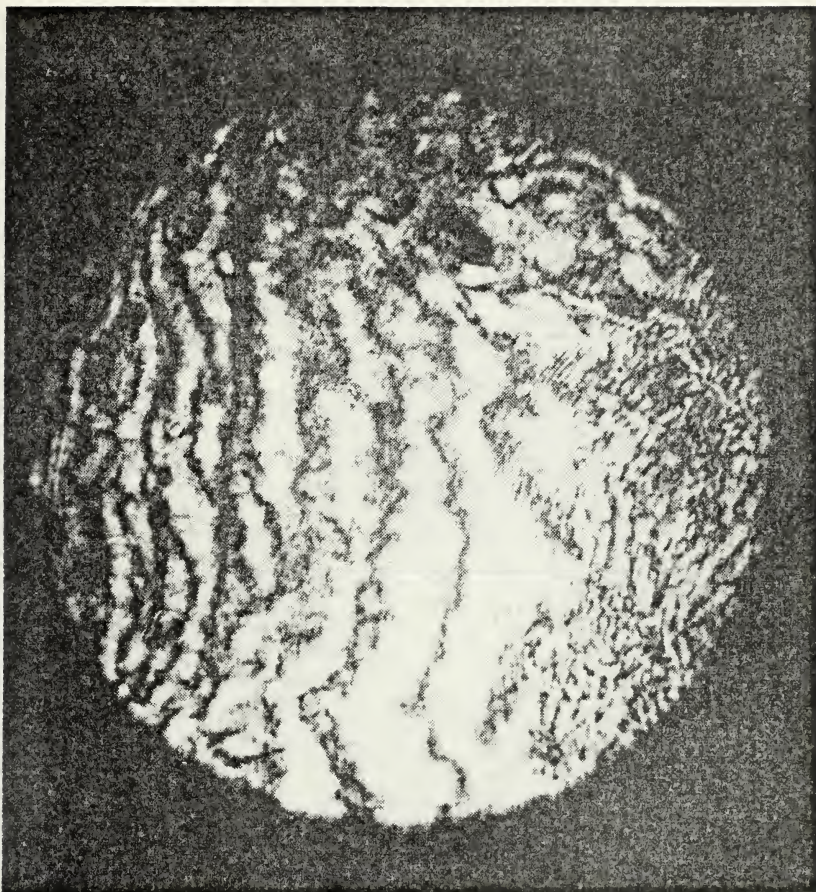


Figure 15. Compression Waves

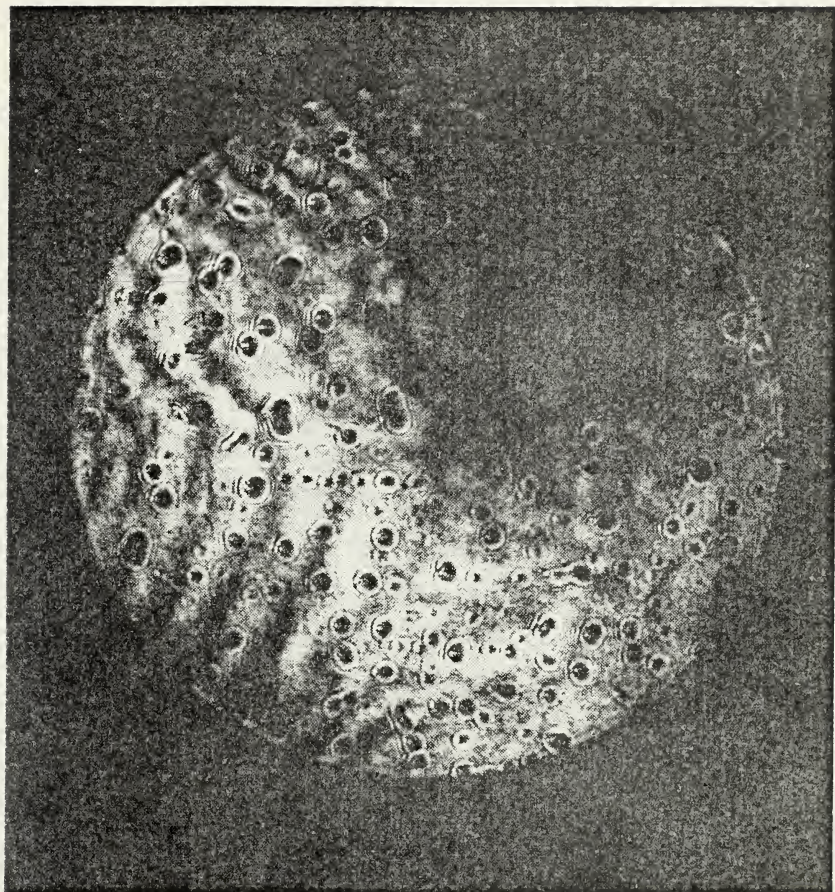


Figure 16. Compression Waves

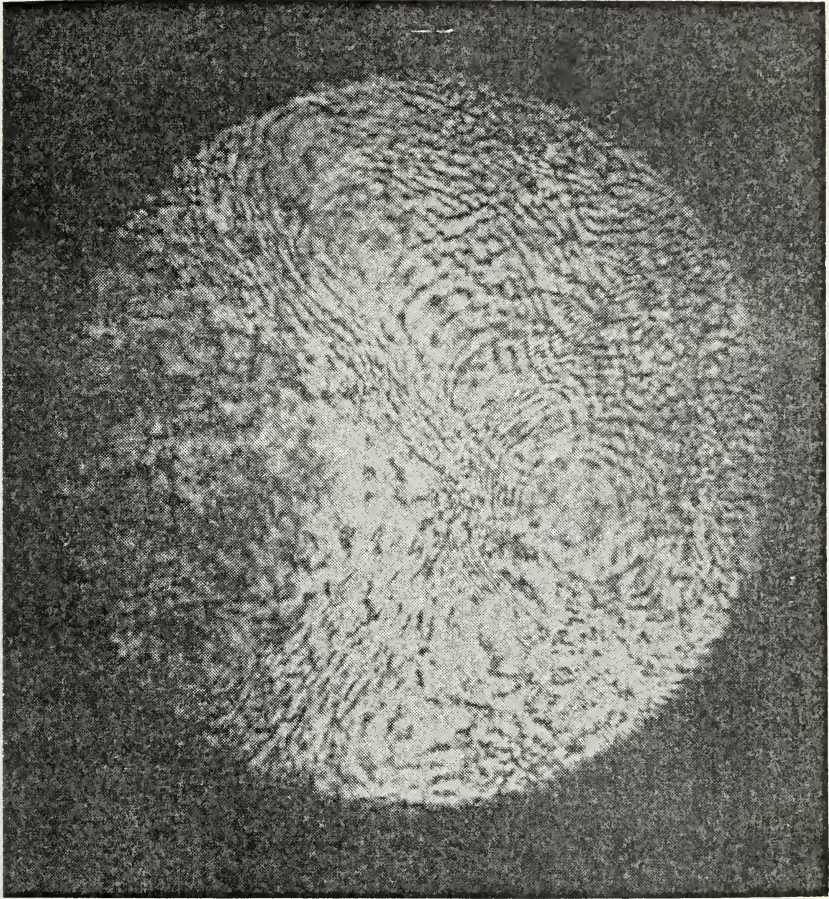


Figure 17. Bow Wave



Figure 18. Hologram Showing Carbon Deposits

GUN BARREL PROJECT

Dimensions: 6 Regions, 6 Zones

<u>Regions</u>	<u>Zones</u>	<u>Length (cm)</u>	<u>Area (cmsq)</u>	<u>Volume (cc)</u>
1	1	1.47	2.95	4.35
2	1	1.47	2.95	4.35
3	1	1.47	2.95	4.35
4	1	1.47	2.95	4.35
5	1	1.47	2.95	4.35
6	1	5.40	2.95	15.93

INITIAL CONDITIONS

Powder Conditions: Grams Powder = 38.23
TBURND = 1.00 Millisec

Materials:

<u>Region</u>	<u>NEQST</u>	<u>Pressure (psi)</u>	<u>Temp. (Deg. K)</u>	<u>Molec. Wt. (gm/mole)</u>
1	2	14.7	300.0	125.00
2	2	14.7	300.0	125.00
3	2	14.7	300.0	125.00
4	2	14.7	300.0	125.00
5	2	14.7	300.0	125.00
6	3	3.0	300.0	55.85

Print out every 0.20 millisec up to 10.00 millisec

Print out every 0.050 millisec up to break

Print out every 0.200 millisec up to launch

Mass of Projectile = 90.0 gm

Break Valve Strength = 690.0 Bars

Number of Pressure Points: 1

Location of Pressure Points: 14.0 cm

Figure 19. Computer Output Format

GUN BARREL PROJECT

Cycle 290	T(Millisecond)	1.88443E00	
	DT(Millisecond)	2.18257E-02	
j	X(CM)	VELOCITY (CM/MS)	PRESSURE (BARS)
1	0.0	0.0	1.01381E 03
2	1.46490E 02	1.01004E 02	8.52849E 02
3	1.47602E 02	1.03653E 02	7.78181E 02
4	1.48734E 02	1.06449E 02	8.85098E 02
5	1.49668E 02	1.07232E 02	1.05442E 03
6	1.50551E 02	1.06399E 02	3.98267E 02

Figure 20. Computer Output Format

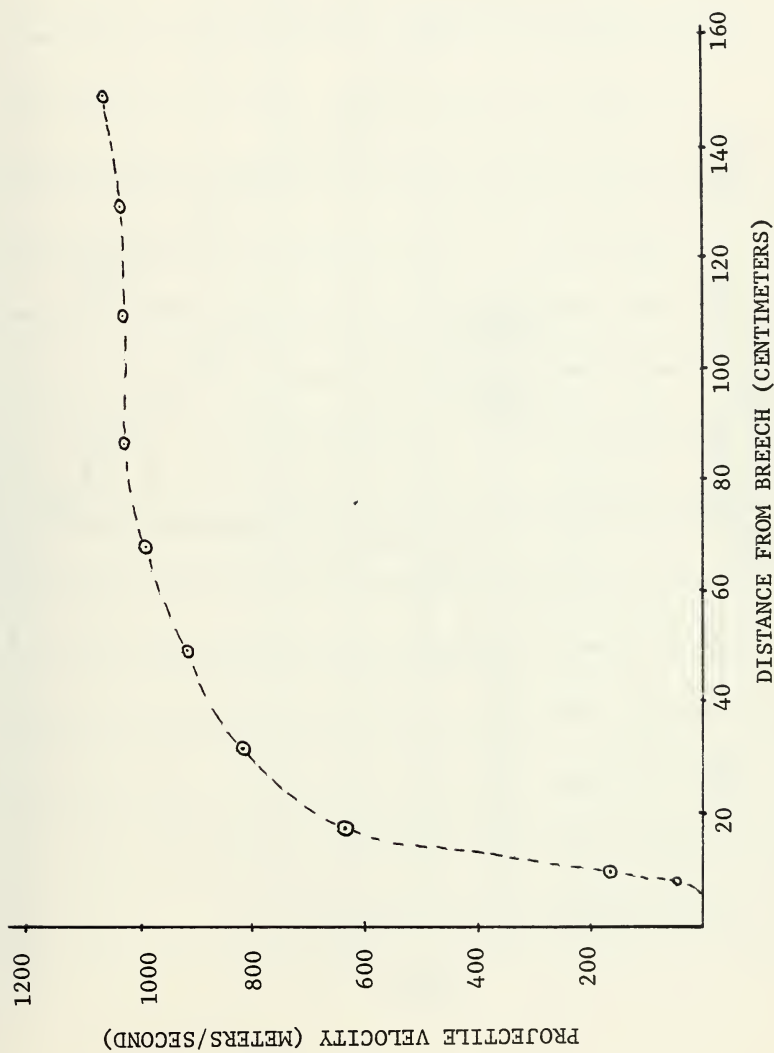


Figure 21. Projectile Velocity vs. Position

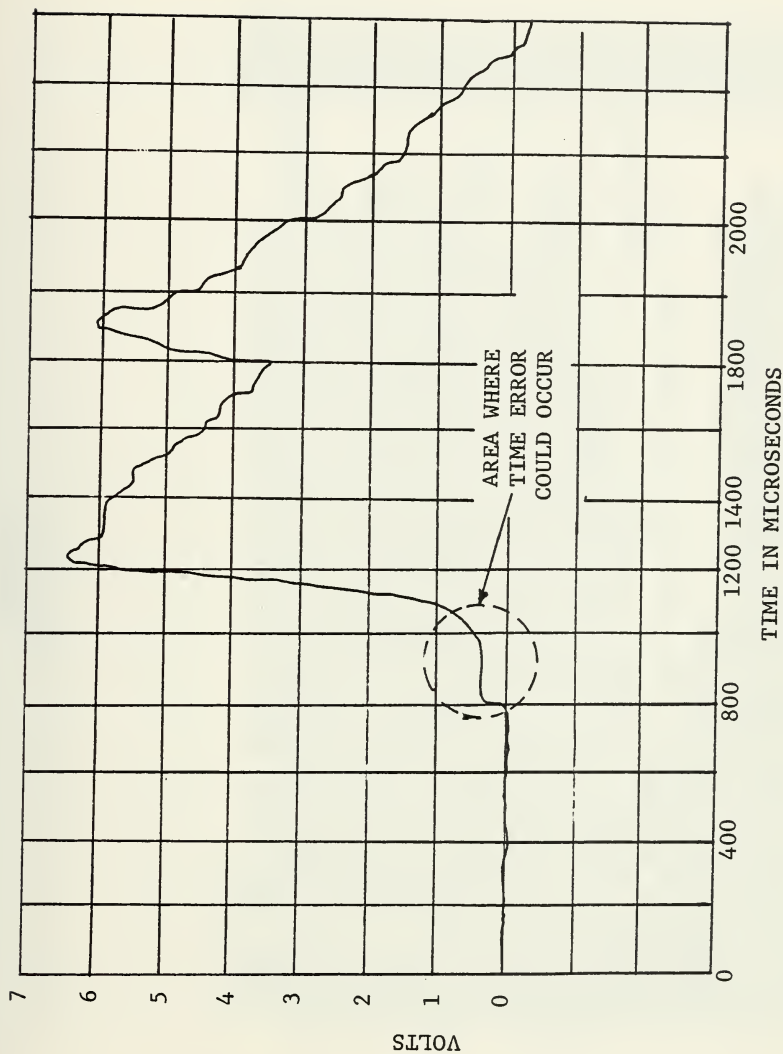


Figure 22. Pressure Trace Output from Pressure Transducer Locate 2.5 inches Aft of Observation Port

GUN PROJECT

61


```

T=0.0
ICATA=0
123 NI=0
M=6
CATA NREAD,NPRINT/5,6/
NVTIR=1
CALL ZEGAB
CALL ZERQA(500,XP1,XP2,PP1,VP2,XP3)
CALL ZERQA(500,PP3,PP1,PP1,PP1)
CALL ZERQA(10,ISTOPX,ISTOPX,ISTOPX,ISTOPX)
INTERJ(31)=M
CPMAX=0.0
PTMAX=0.0
ANEMAX=0.0
NTIMPT=0
IP=0
NPNCH=1
IPNCHX=0
LN=0
IPV1=1
IPV2=2
C INITIAL CONDITIONS FOR PROGRAM, BEGIN INPUT FOR RUN,NEW OR ITE
IF(NPVTIR.EQ.1)GO TO 41
NVTIR=1
INPUT FOR ITERATION FROM STORAGE
C 620 CALL STORC(ISTORM, STORM)
EMLEAD=STORM(97)
HYDRD1=STORM(98)
HYDRD2=STORM(99)
NEQST(30)=ISTORM(100)
IF(ICATA)8,8,608
C 41 CONTINUE
INPUT FOR NEW RUN, STORAGE OF INPUT
C READ(NREAD,604)ICATA,IPRNTZ,ITRNSF,IPUNCH,DTSQ(199)
604 IF(ITERNSF.EQ.0) GO TO 619
M=6
INTERJ(31)=M
619 IF(ICATA)606,606,620
608 IF(ITERNSF.EQ.0) GO TO 619
M=6
GO TO 610
610 CALL READ
READ(NREAD,20) IPOX, NPOX, (XPO(M), M=1, NPOX)
READ(NREAD,49) XPV1, XPV2, PVERR, PVWANT
READ(NREAD,61R,EMPIST, FRAC, EMLEAD
6 FORMAT(E10.4,3F10.0)
6 READ (NREAD,49) (AMOL(I),I=1,IMAX)
GUNN0037
GUNN0038
GUNN0039
GUNN0040
GUNN0041
GUNN0042
GUNN0043
GUNN0044
GUNN0045
GUNN0046
GUNN0047
GUNN0048
GUNN0049
GUNN0050
GUNN0051
GUNN0052
GUNN0053
GUNN0054
GUNN0055
GUNN0056
GUNN0057
GUNN0058
GUNN0059
GUNN0060
GUNN0061
GUNN0062
GUNN0063
GUNN0064
GUNN0065
GUNN0066
GUNN0067
GUNN0068
GUNN0069
GUNN0070
GUNN0071
GUNN0072
GUNN0073
GUNN0074
GUNN0075
GUNN0076
GUNN0077
GUNN0078
GUNN0079
GUNN0080
GUNN0081
GUNN0082
GUNN0083
GUNN0086

```



```

      READ (NREAD,49) (TO(I),I=1,IMAX)
      READ (NREAD,49) (PO(I),I=1,IMAX)
      FORMAT(7F10.0)
      49
610 CONTINUE
      CALL STORIN (ISTORM, STORM)
      STORM(97)=EMLEAD
      STORM(98)=HYDR01
      STORM(99)=HYDR02
      ISTORM(100)=IPOX
      INITIAL CONDITIONS AND CONSTANTS FOR RUN
      8 NPIN=NZONES(1)+NZONES(2)+NZONES(3)+1
      XSTT=FRAC*OUTBDY(5)
      NEGST(30)=IPOX
      616 CALL CALCUL (EMLEAD)
      IF (N1.NE.0) GO TO 603
      CALL PRINT(EMLEAD,FRAC,XPV1,XPV2,PVWANT,NPCX,IPCX,XPG)
      IF (IPRNTZ.EQ.0) GO TO 603
      READ(NREAD,11) ILASTK
      IF (ILASTK) 123,12,1
      603 CALL SETUP
      DO 706 IMP=1, JLAST
      PMDMIN(IMP)=PPLUSQ(IMP)
      PMDMAX(IMP)=PPLUSQ(IMP)
      706 MAIN LOOP OF PROGRAM - DYN,REQ, LFTOVER, AND OUTPUT
      2 CALL DYNREQ
      CALL LFTQVR(IPNCHX)
      DO 710 IMP=1, JLAST
      IF (PPLUSQ(IMP).GT.PMDMIN(IMP)) GO TO 705
      PMDMIN(IMP)=PPLUSQ(IMP)
      PMDMIN(IMP)=T
      705 IF (PPLUSQ(IMP).LT.PMDMAX(IMP)) GO TO 710
      PMDMAX(IMP)=PPLUSQ(IMP)
      PMDMAX(IMP)=T
      710 CONTINUE
      IF (IPUNCH.EQ.0 .OR. JPROJ.NE.300) GO TO 627
      PRSTAB(NPUNCH)=T-DTSQ(200)
      NPNI=NPUNCH+1
      JPLTAF=INTERJ(6)
      J=JPLHAF
      JMNHAF=JPLHAF-1
      DUDI=26./18.*PPLUSQ(JMNHAF)-1./9.*PPLUSQ(JMNHAF-1)
      707 PRSTAB(NPNI)=DUDI
      IF (T.GT.(DTSQ(200)+DTSQ(199))) GO TO 647
      PRSTAB(NPNI)=PRSTAB(NPNI)*(T-DTSQ(200))/DTSQ(199)
      647 NPUNCH=NPUNCH+2
      625 IF (51-NPUNCH) 625, 625, 627
      PUNCH_641 PRSTAB
      641 FORMAT(3F12.8,E12.8))

```



```

NPUNCH=1
627 CONTINUE
630 M=6
72 C
C CONTINUE OF MAXIMUM PRESSURES
  INER51 = INTERJ(6) -1
  CPMAX = MAX1(CPMAX, PPLUSQ(NPTN-1))
  PPMAX = MAX1(PPMAX, PPLUSQ(INER51))
  AMPMAX = MAX1(AMPMAX, PPLUSQ(INER51))
  DETERMINATION IF MODEL HAS BEEN LAUNCHED
  IF(XSTOP-X(JLAST,NPLUS1)) 9, 3, 3
  C
  C ROUTINE STORAGE OF POINTS TO BE PLOTTED
  3 IF(IPOX.EQ.5) GO TO 2
    IF (X(INPTN, N) . LT . XSST ) GO TO 2
    KN=NCYCLE/6
    CN=NCYCLE
    TN=SN/6
    IF(TN-UN) 4, 4, 2
    4 IF(LN-GT.498) GO TO 7
      LN = LN + 1
      IF (IPOX.EQ.6) GO TO 75
      XP3(LN)=T
      PP3(LN)=PPLUSQ(NPTN)
      XP4(LN)=X(NPTN-1,N)
      PP4(LN)=PPLUSQ(NPTN-1)
      IF(IPOX.EQ.1) GO TO 51
      DO 60 INPOX=1, NPOX
        IF(ISTOPX(INPOX).GE.1) GO TO 60
        NIMPT=LN
        DC 58 INPTN=2, JLAST1
        58 CONTINUE
        IF(XPO(INPOX).LT.X1(INPTN)) GO TO 59
        DUMVAR(LN, INPOX)=PPLUSQ(INER51)
        NPTPL(INPOX)=LN
        GO TO 60
        59 DUMVAR(LN, INPOX)=PPLUSQ(INPTN-1)+(PPLUSQ(INPTN-1)-PPLUSQ(INPTN))
          1/(X1(INPTN-1)-X1(INPTN))*(XPO(INPOX)-X1(INPTN-1))
          NPTPL(INPOX)=LN
          IF(LN.EC.1099)GO TO 55
          GO TO 60
          55 ISTOPX(INPOX)=2
            NPTPL(INPOX)=LN
            CONTINUE
            60 IF (IPOX.NE.6) GO TO 78
              75 DUMVAR(LN,1)=PPLUSQ(INER51)
              78 IPOX(LN)=1
                IF (IPOX.EQ.6) GO TO 2

```

GUNNO133
 GUNNO134
 GUNNO135
 GUNNO136
 GUNNO137
 GUNNO138
 GUNNO139
 GUNNO140
 GUNNO141
 GUNNO142
 GUNNO143
 GUNNO144
 GUNNO145
 GUNNO146
 GUNNO147
 GUNNO148
 GUNNO149
 GUNNO150
 GUNNO151
 GUNNO152
 GUNNO153
 GUNNO154
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 GUNNO156
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 GUNNO162
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 GUNNO167
 GUNNO168
 GUNNO169
 GUNNO170
 GUNNO171
 GUNNO172
 GUNNO173
 GUNNO174
 GUNNO175
 GUNNO176
 GUNNO177
 GUNNO178
 GUNNO179
 GUNNO180


```

51 IF(IPOX.EQ.2) GO TO 52
C PROGRAM TO FIND MAX IN REGION TO GO HERE
52 CONTINUE
C STORAGE OF MODEL PLOTS AFTER BREAK VALVE
7 IF(JPROJ-300) 13,5,13
5 IF(IP.GT.498) GO TO 2
IP=IP+1
IF(XSTOP.EQ.3000.) GO TO 76
10 XP(IP)=X(JLAST,N)
XP2(IP)=X(JLAST,N)
PP1(IP)=PPUSQ(INER51)
VP2(IP)=U(JLAST, NMNHAF)
13 GO TO 2
C POINT OF RETURN TO MAIN LOOP OF PROGRAM
C FINAL STORAGE OF POINTS TO BE PLOTTED, AND WRITING OF ALL PLOT TAPES
9 IF (IPOX.EQ.5) GO TO 25
IF (IPOX.EQ.6) GO TO 76
IP=IP+1
XP(IP)=X(JLAST,N)
XP2(IP)=X(JLAST,N)
PP1(IP)=PPUSQ(INER51)
VP2(IP)=U(JLAST, NMNHAF)
GO TO 36
35 NPOX=1
36 DO 70 IPLTXT=1,NPOX
NPTIX=NPTPL(IPLTXT)
IF(NPTIX.LT.10) GO TO 70
NPTT=NPTPL(IPLTXT)
DO 80 ITP=1,NPTT
IPL(IITP)=IPOX(ITXP)
PPLT(ITXP)=DUMVAR(ITXP, IPLTXT)
80 IF(JPROJ.NE.300) GO TO 1
70 CONTINUE
GO TO 25
76 DO 93 ITP=1, LN
93 PPLT(ITXP)=DUMVAR (ITXP,1)
C TERMINATION OF RUN RETURN FOR NEW INPUT
25 READ(INREAD,1) ILASTK
IF((IPUNCH.EQ.0).OR.(NPUNCH.EQ.1)) GO TO 629
NPUNCH=NPUNCH+1
PUNCH 641, (PRSTAB(IPXX), IPXX=1,NPUNCH)
625 CONTINUE
WRITE(6,704) ((IT,PMDMIN(IT),TMDMAX(IT),TMDMAX(IT)
1 IT=1,JLAST)
704 FORMAT(132X,E12.6,2X,E12.6,2X,E12.6)
45 FORMAT(3F20.2)
IF(ILASTK) 15, 12, 1

```

GUNNO181
GUNNO182
GUNNO183
GUNNO184
GUNNO185
GUNNO186
GUNNO187
GUNNO188
GUNNO189
GUNNO190
GUNNO191
GUNNO192
GUNNO193
GUNNO194
GUNNO195
GUNNO196
GUNNO197
GUNNO198
GUNNO199
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GUNNO209
GUNNO210
GUNNO211
GUNNO212
GUNNO213
GUNNO214
GUNNO215
GUNNO216
GUNNO217
GUNNO218
GUNNO219
GUNNO220
GUNNO221
GUNNO222
GUNNO223
GUNNO224
GUNNO225
GUNNO226
GUNNO227
GUNNO228


```

WRITE (6,103) I,NZONES(I),XLGTH(I),AREAL,REGVOL(I)
IF (IMAX.EQ.1) GO TO 211
KQX=IMAX-1
WRITE (6,103) (I,NZONES(I),XLGTH(I),AREA2,REGVOL(I),I=2,KQX)
WRITE (6,103) IMAX,NZONES(IMAX),XLGTH(IMAX),AREA3,REGVOL(IMAX)
WRITE (6,105) SLOPE,ANGLE
WRITE (6,111) CALPGM,TBURND,GMSPCR,GASPRS
WRITE (6,106)
WRITE (6,108) (I,NEQST(I),PO(I),TO(I),AMOL(I),CQSQX4(I),I=1,IMAX)
WRITE (6,109)
WRITE (6,110) (I,GAMMA(I),EZERO(I),ROZERO(I),VZERO(I),I=1,IMAX)
WRITE (6,110) R
WRITE (6,124) XPV1,XPV2,PVWANT
WRITE (6,114) OUTDT1,TMAX1,OUTDT2,TMAX2
WRITE (6,115) EMLEAD*453.59
EMLEAX=EMLEAD*453.59
EMPISX=EMPISX*453.59
XXMAS=REGVOL(IMAX)*ROZERO(IMAX)
SHPRX=SHPR*14.504
WRITE (6,112) EMLEAD,EMLEAX,EMPISX,XXMAS
WRITE (6,113) SHPR,SHPRX
KQX=IPOX+1
GO TO (10,11,12,12,13,14),KQX
10 WRITE (6,119) IPOX
GC TO 15
11 WRITE (6,120) IPOX
GC TO 15
12 WRITE (6,123) IPOX
GC TO 15
13 WRITE (6,121) IPOX
GC TO 15
14 WRITE (6,122) IPOX
15 WRITE (6,116) NPOX
WRITE (6,117) (XPO(I),I=1,NPOX)
WRITE (6,118) FRAC
WRITE (6,65)
RETURN
100 FORMAT (23X,36HYPERVELOCITY MODEL LAUNCHER PROGRAM//22X,19HCOMPUTE)
101 RUN NUMBER,15,7H DATE,12,1H,12,1H,121
102 FORMAT (1H/34X,14HGUN DIMENSIONS/31X,12,10H REGIONS ,13,6H ZONES/GUNNO303
1//12X,6HREGION,5X,5HZONES,6X,6HLENGTH,9X,4HAREA,11X,6HVOLUME/35X,4G
2H(CM) 9X,6H(CMSQ),11X,4H(CCC)/1H)
103 FCMAT (14X,12,9X,12,2X,F10.2,5X,F10.2,7X,F10.2)
104 FORMAT (14X,12,9X,12,2X,F10.2,11X,3H---,12X,3H---)
105 FORMAT (1H/19X,7HSLOPE =,F8.4,9X,7HANGLE =,F6.2,5H DEG)
106 FORMAT (1H/5X,12HATERIALS --//7X,6HREGION,5X,5HNEQST,5X,8HPRESSURE/GUNNO309
1E7X,4HTEMP,9X,8HMOLEC WT,6X,6HCSQX4/30X,5F(PST,16X,17H(DEG K),7X,
25F(GM/MOLE)/1H)
108 FORMAT (9X,12,8X,12,5X,F9.2,6X,F7.2,6X,F9.4,6X,F5.1)

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109 FORMAT(1H /6X,6HREGION,4X,5HGAMMA,9X,6HENERGY,10X,7HDENSITY,9X,9HSGUNNO373
1P VOLUME/26X,13H(BARS-CC/CCO),7X,7H(GM/CC),5X,8H(CC/CCO)/1H )
GUNNO374
110 FORMAT(8X,12,5X, F6.3,6X, E11.4,5X,E11.4,6X,E11.4)
GUNNO375
111 FORMAT(1H //32X,18HINITIAL CONDITIONS/5X,20HPOWDER CONDITIONS --//GUNNO376
114X,8HCA PCM =,F12.4,6X,8HTBURND =,F12.4,6H MSEC/14X,8HGMSPDR =,F12.4,6X,8HPSI)
GUNNO377
112 FORMAT(1H //5X,10HWEIGHTS --//9X,6HPHISTON/13X,23HMASS OF FIRST SECT/GUNNO379
11CN =,F13.4,4H LB,8X,1H=,F13.4,4H GM/13X,24HMASS OF SECOND SECT/GUNNO380
20N =,F12.4,4H LB,8X,1H=,F13.4,4H GM//9X,15HMODEL/13X,15HPASS OF /GUNNO381
30DEL =,F12.4,4H CM)
GUNNO382
113 FORMAT(1H //18X,22HBREAK VALVE STRENGTH =,F10.2,6H BARS,5X,1H=,F10.2,6H
1.2,5H PSI)
GUNNO383
114 FCFORMAT(1H //5X,18HPHISTON VELOCITY --//10X,6HXPV1 =,F10.2,7H CM
110X,6HXPV2 =,F10.2,7H CM /10X,18HDESIRED VELOCITY =,F10.2,7H FT/GUNNO385
2/SEC)
GUNNO386
115 FCFORMAT(2H //20X,15HPRINT OUT EVERY,F7.3,11H MSEC UP TO,F7.3,5H MSEC/GUNNO388
1EC/20X,15HPRINT OUT EVERY,F7.3,17H MSEC UP TO BREAK/20X,15HPRINT OUT/GUNNO389
2UI EVERY,F7.3,18H MSEC UP TO LAUNCH)
GUNNO390
116 FCFORMAT(1H //10X,26HNUMBER OF PRESSURE POINTS ,14//10X,27HLOCATION OFGUNNO391
1F PRESSURE POINTS)
GUNNO392
117 FCFORMAT(20X,F9.2,3H CM) START FRACTION ,1PE11.4)
GUNNO393
118 FCFORMAT(1H //10X,20HPLOT --,10X,6HIPOX =,13.34H (ALL PLOTS, ALL PRES/GUNNO394
119 FCFORMAT(1H //5X,8HPLOTS --,10X,6HIPOX =,13.34H (ALL PLOTS, NO PRES/GUNNO395
1SSURE POINTS))
GUNNO396
120 FCFORMAT(1H //5X,8HPLOTS --,10X,6HIPOX =,13.34H (ALL PLOTS, NO PRES/GUNNO397
1SSURE POINTS))
GUNNO398
121 FCFORMAT(1H //5X,8HPLOTS --,10X,6HIPOX =,13.12H (NO PLOTS))
GUNNO399
122 FCFORMAT(1H //5X,8HPLOTS --,10X,6HIPOX =,13.24H (ONLY PRESSURE POIN/GUNNO400
1TS))
GUNNO401
123 FCFORMAT(1H //5X,8HPLOTS --,10X,6HIPOX =,13)
GUNNO402
124 FCFORMAT(1H //6X,3HR =,1PE11.4)
GUNNO403
END
GUNNO404
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5 SKIN(200),TSIGSQ(200),TMINSQ(2),TOVREI(30),THETA(200),UZERO(30),
6 U(201,2),USQ(201),VZERO(30),V(200,2),VISCOS(200),X(201,2),XI(200),
7 ZMSSQ(200),PO(30),I(30),AMOL(30),DUNVAR(500,5)
8 DTLAST=DTMIN(NPLHAF)
9 M=INTERJ(31)
10 IF(SIGMAX.EQ.0.0)GO TO 240
11 SIGMIN=1./SIGMAX
12 GC TO 244
13 SIGMIN=0.0
14 IF(SIGMIN-7.41*TMINSQ(NPLHAF)) 270,270,250
15 IF(DLAMAX-.079) 255,270,270
16 IF(SIGMIN-1.1*TMINSQ(NPLHAF)) 265,260,260
17 IF(DLAMAX-.085) 270,270,265
18 TMINSQ(NPL3HF)=TMINSQ(NPLHAF)
19 GC TO 285
20 IF(DLAMAX-.01) 275,275,280
21 TMINSQ(NPL3HF)=SIGMIN/2.25
22 GC TO 285
23 TMINSQ(NPL3HF)=AMINI(SIGMIN/9.00,.005184*TMINSQ(NPLHAF)/DLAMAX**2)
24 DTMIN(NPL3HF)=AMINI(SORT(TMINSQ(NPL3HF)),1.4*DTMIN(NPLHAF))
25 DTMIN(NN)=(DTMIN(NPL3HF)+DTMIN(NPLHAF))/2.
26 NP=NPLUS1
27 NPLUS1=N
28 NPLHAF=NPLUS1
29 N=NP
30 NMNHAF=N
31 NPL3HF=N
32 EINSUM=0.
33 EKSUM=0.
34 USQ(1)=0.(1,N)**2
35 DO 300 I=1,IMAX
36 EINT(I)=0.
37 EKIN(I)=0.
38 JMAX=INTERJ(I+1)-1
39 JMIN=INTERJ(I)
40 DO 295 J=JMIN,JMAX
41 JPLHAF=J
42 USQ(J+1)=U(J+1,N)**2
43 XI(JPLHAF)=(X(J,N)+X(J+1,N))/2.
44 EINT(I)=EINT(I)+E(JPLHAF,N)/HALFRO(I)*HALFM(JPLHAF)
45 EKIN(I)=(USQ(J)+USQ(J+1))*HALFM(JPLHAF)+EKIN(I)
46 EKIN(I)=5*EKIN(I)
47 EINSUM=EINSUM+EINT(I)
48 EKSUM=EKSUM+5*EINT(I)
49 EKSUM(6)=5*EMPROJ*U(JLAST,NMNHAF)**2+EKIN(6)
50 EKSUM=5*EMPROJ*U(JLAST,NMNHAF)**2+EKSUM
51 EKSUM=EINSUM+EKSUM
52 EKSUM=EINSUM+EKSUM
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49 WRITE(M,IJK,NUMBER,NDATE1,NDATE2,NDATE3
51 WRITE(M,12)
52 WRITE(M,6) NCYCLE,I,DTLAST,ESUM
53 IF(NCYCLE) 53,53,400
54 DC 57 JPLHAF=1,JLAST1
57 ZMASS(JPLHAF)=2.* HALF(M(JPLHAF)
60 WRITE(M,2)
WRITE(M,3)
WRITE(M,5555)
DO 602 IL=1,JLAST1
DO 602 IL=2,I LIMIT
IF(L=INTERJ(IL)) 602,603,602
602 CONTINUE
WRITE(M,4) L,X(L,N),U(L,NMNHAF),V(L,N),PPLUSQ(L),Q(L,NMNHAF),
1E(L,N),AREA(L,N),DTSQ(L),ZMASS(L)
GC TO 604
603 WRITE(M,5556)
5556 FORMAT(IHO)
WRITE(M,4) L,X(L,N),U(L,NMNHAF),V(L,N),PPLUSQ(L),Q(L,NMNHAF),
1E(L,N),AREA(L,N),DTSQ(L),ZMASS(L)
604 CCNTINUE
WRITE(M,4) JLAST,X(JLAST,N),U(JLAST,NMNHAF)
GC TO 71
400 NYCRAC=HYDRD2
IF((NYDRA2.EQ.0).OR.((NYDRA2-60).EQ.0).OR.((NYDRA2-30).EQ.0))
1 GO TO 100
IF((NYDRA2.GT.30).AND.(NYDRA2.LT.60)) GO TO 300
IF(NYDRA2.GT.60) GO TO 600
NZN=1
NZM=INTERJ(NYDRA2+1)-1
GO TO 200
300 NYCRAC=NYDRA2-30
NZN=INTERJ(NYDRA2)
NZM=INTERJ(NYDRA2+1)-1
GC TO 200
600 NYDRA2=NYDRA2-60
NZN=INTERJ(NYDRA2)
NZM=JLAST1
DO 70 JK=NZN,MZM
JKN=JK-NZN+1
XP6(JKN)=X1(JK)
XP6(JKM)=U(JK,NMNHAF)/100.
XP5(JKM)=X1(JK)
PP5(JKM)=PPLUSQ(JK)
70 CCNTINUE
WRITE(M,7)
100 WRITE(M,8)
WRITE(M,5555)

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DO 704 L=1,JLAST1
DO 702 L=2,IJLIMI
IF(L,N)TERJ(1L) 702,703,702
702 CCNITNUE 4) L,X(L,N),U(L,NMNHAF),V(L,N),PPLUSQ(L),Q(L,NMNHAF),
WRITE(M,4) AREA(L,N),DTSQ(L),X1(L)
1E(L,N),AREA(L,N),DTSQ(L),X1(L)
GC TO 704
703 WRITE(M,5555)
FORMAT(1H)
5555 WRITE(M,4) L,X(L,N),U(L,NMNHAF),V(L,N),PPLUSQ(L),Q(L,NMNHAF),
1E(L,N),AREA(L,N),DTSQ(L),X1(L)
704 CCNITNUE 4) JLAST,X(JLAST,N),U(JLAST,NMNHAF)
WRITE(M,9)
71 WRITE(M,10) (I,NEQST(I),EKINI),EINT(I),I=1,IMAX)
75 WRITE(M,6) NCYCLE,I,DTLAST,ESUM
WRITE(M,5)
5 FORMAT(1H)
IF(ENWRONG) 95,95,80
80 WRITE(M,11)
95 RETURN
9555 FORMAT(115,1P7E13.5) H V MODEL LAUNCHER(413)
1EFORMAT(5X,12-20H J X(J,N) U(J,N-1/2) V(J+1/2,N) P(J+1/2,N)
2 FCRMAT(118H0 J X(J,N) AREA(J,N) DTSQ(1/2,1/2) DM(J+1/2)
1) Q(J+1/2,N-1/2) E(J+1/2,N) CM/MILLISEC CC/CCO GRAMS)
3 FCRMAT(114H CM/MILLISEC MILLISECSQ
1 BARS BARS-CC/CCO
4 FCRMAT(14,1P6E13.5,2E11.3,E13.5)
6 FCRMAT(15,1P3E15.5) U(J,N-1/2) V(J+1/2,N) P(J+1/2,N)
7 FCRMAT(119H0 J X(J,N) AREA(J,N) DTSQ(1/2,1/2) X(J+1/2,N)
1) Q(J+1/2,N-1/2) E(J+1/2,N) CM/MILLISEC CC/CCO CM)
8 FCRMAT(114H CM/MILLISEC MILLISECSQ CM)
1 BARS BARS-CC/CCO K-ENERGY I-ENERGY)
9 FCRMAT(46HOREGION MATERIAL CM)
10 FCRMAT(15,18, 2E15.5) ENERGY CHECK)
11 FCRMAT(53H1 TOTAL E)
12 FCRMAT(47HOCYCLE T DT
END
SLEROUTINES INITIAL REGIONAL ENERGY SPECIFIC VOLUME AND DENSITY
CALCULATES INITIAL REGIONAL ENERGY SPECIFIC VOLUME AND DENSITY
COMMON PCON3,SLOPE,RADIUS,CALPGM,TBURND,GMSPRD,GASPRS,IHEL
COMMON AREA1,AREA2,AREA3,AREA4,CSCX4,CSCMAX,CPCV,DLAMAX,GUNNO653
1,DTMIN,DUDT,DLAMDA,DTSQ,DTLAST,DJLAST,DZLAST,DELX,CMU,DPDE,GUNNO654
2EPCMU,Q1,Q2,Q3,EZERO,EINSUM,ESUM,EINT,EKIN,EETOT,EIENH,GUNNO655
3EWRONG,E1,FORCE,GAMMA,HALFUM,HALFRO,HYDRD1,HYDRD2,HYDRD3,HYDRAD,GUNNO656
4QUITBDY,QUITD1,QUIT2,PCON1,PCON2,VDI1,TVDI2,I,PMAX,ISISQ,SHPR,GUNNO657
5SIGTMAX,SIGMIN,SKIN,TMAX,TMIN,TMINSQ,TVREQ,UZERO,U,USQ,TBAR,TOVRE1,THETA,TWALL,GUNNO658
6TPRINT,TVNEXT,TMINSQ,TVREQ,UZERO,U,USQ,TBAR,TOVRE1,THETA,TWALL,GUNNO659
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7VZERO,V,VOLUME,VISCOS,X,X1,XGRID,XMIN,XMAX,ZMASS,EMPROJ,XSTOP
COMMON,IMAX,INU,1,INTER,1,1,INDEX,1,1,IMAX1,K,X,L,MACHSQ,NDATA1,NDAT,E2,
1JPLHAF,JMNHAF,PLAST,1,1,1,JMIN1,JMAX1,K,X,L,MACHSQ,NDATA1,NDAT,E2,
2NCATE3,NUMBER,NTV,NCKEKE,NQST,NZONES,NCKELE,N,NMNAF,NPLUS1,
3NPLHAF,NN,NPL3H,NP,I,QUIT,JPROJ,JSTOP,R,EMPIST,PO,TO,AMOL,DUMVAR
DIMENS(3) AREA1(200,2),COSQX4(30),CMAXR(30),CSQ(200),CP(30),CV(30),
1DIMIN(3) ALAMD(200,2),DTSQ(200),DELX(30),DO1(200),DQ2(200),DS(200),
2EZERO(30),E(200,2),E1,NIT(30),EK,NIT(30),FORC(200),GAMMA(30),
3HALFEM(200),HALFPC(30),HYDRAD(200),INTERJ(30),MACHSQ(200),NEQST(30),
4NZONES(30),OUTBODY(30),HPLUSQ(200),P(200,2),Q(200,2),ROZERO(30),
5KIN(200),TSIGSQ(200),TMINSQ(2),TQVKEI(30),TETA(200),UZERO(30),
6U(201,2),USQ(201),VZERO(30),V(200,2),VISCOS(200),X(201,2),X1(200),
7ZMASS(200),PO(30),TO(30),AMOL(30),DUMVAR(500,5)
M=INTERJ(31)
DO 50 I=1,IMAX
  CZERO(I)=AMOL(I)/22.4E3
  EZERO(I)=R*TO(1)/PO(I)/AMOL(I)*14.5/1,E6=ROZERO(I)
  VZERO(I)=PO(I)*VZERO(I)/(GAMMA(I)-1)/14.5
  WRITE(M,21)
  FORMAT(1H)
  DO 25 IK=1,IMAX
    IF (PO(IK).NE.1.0) GO TO 23
    IF (GAMMA(IK)=1.
      VZERO(IK)=0.
      EZERO(IK)=1.0
      CZERO(IK)=EMLEAD*453.7/(AREA2*(OUTBODY(2)-OUTBODY(1)))
      IF (PO(IK).NE.2.0) GO TO 24
      IF (GAMMA(IK)=1.
        EZERO(IK)=1.0
        CZERO(IK)=1.0
        VZERO(IK)=1.0
      VZERO(IK)=EMPIST*453.7/(AREA2*(OUTBODY(3)-OUTBODY(2)))
      IF (PO(IK).NE.3.0) GO TO 25
      IF (GAMMA(IK)=1.
        EZERO(IK)=1.0
        CZERO(IK)=1.0
        VZERO(IK)=1.0
      VZERO(IK)=EMPROJ/(AREA3*(OUTBODY(6)-OUTBODY(5)))
      EMPROJ=0.0
      ROZERO(IK)=0
      KMPROJ=0
      CONTINUE
      RETURN
    END
  SUBROUTINE ZEAB
  ZEROS ALL VARIABLES BETWEEN RUNS
  COMMON PCON3,SLOPE,RADIUS,CALPGM,TBURND,CMS,PDR,GASPRS,IHEL,X
  COMMON AREA1,AREA2,AREA3,AREA4,REAT,CQ,CQX1,CMAXR,CSQ,COSMAX,CP,CV,DLAMA
  COMMON AREA1,ALB,AREA2,DTSQ,DTLAST,DUMJ,DTLAST,CNZGME,DELX,DELXT,DPDE,
  1,DTMIN,OUTD,DLAMD,DTSQ,DTLAST,DUMJ,DTLAST,CNZGME,DELX,DELXT,DPDE,
  2,DPDMN,DQ1,DQ2,D3,EZERO,EENSUM,E,SUM,EKSUM,INT,EK,TN,E,DETOT,ETENTH,
  3EWRONG,E1,FORCE,GAMMA,HALFM,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  4OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  5OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  6OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  7OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  8OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  9OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  10OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  11OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  12OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  13OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  14OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  15OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  16OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  17OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  18OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  19OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  20OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  21OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  22OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  23OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  24OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  25OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  26OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  27OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  28OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  29OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  30OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  31OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  32OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  33OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  34OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  35OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  36OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  37OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  38OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  39OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  40OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  41OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  42OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  43OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  44OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  45OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  46OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  47OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  48OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  49OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  50OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  51OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  52OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  53OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  54OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  55OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  56OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  57OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  58OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  59OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  60OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  61OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  62OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  63OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  64OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  65OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  66OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  67OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  68OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  69OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  70OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  71OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  72OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  73OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  74OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  75OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  76OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  77OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  78OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  79OUTBODY,OUTD1,OUTD12,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZERO,SHPR,
  80OUTBODY,OUTD1,OUT
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GUNN0709 T, TMAX, TSIGSQ, TNEXT)
GUNN0710 I, TOVREL, THETA, WALL,
GUNN0711 ZMASS, ZMEMP, PROJ, XSTOP
GUNN0712 J, PROJ, JPROJQ2, JMIN, JMAX, J,
GUNN0713 K, L, MACHSQ, NDAT, E2,
GUNN0714 N, NMHAF, NPLUS1,
GUNN0715 P, PO, TO, AMOL, DUMVAR,
GUNN0716 CP(30), CV(30),
GUNN0717 C(200), PQ2(200), DS(200),
GUNN0718 GAMMA(30),
GUNN0719 MACHSQ(200), MEQST(30),
GUNN0720 ROZRO(30),
GUNN0721 THETA(200), UZERO(30),
GUNN0722 X(201, 2), X1(200),
GUNN0723 DUMVAR(500, 5)
GUNN0724 DTLAST, DLAST1)
GUNN0725 ESUM, EKSUM,
GUNN0726 HYDRD2, HYDRD3, OUTOTL1)
GUNN0727 SIGMA, SIGMIN, IMAX1)
GUNN0728 IMPRINT, TVNEXT)
GUNN0729 XGRID, XMIN, XMAX, EMPROJ)
GUNN0730 JPROJ, JPROJQ2)
GUNN0731 JLAST1, JMIN1)
GUNN0732 NUMBER, NTV)
GUNN0733 NPLUS1, NPL3HF)
GUNN0734
GUNN0735
GUNN0736
GUNN0737 R)
GUNN0738
GUNN0739
GUNN0740 ROZREL)
GUNN0741
GUNN0742
GUNN0743 INTERJ, INTERJ)
GUNN0744 TOVREL, TOVREI)
GUNN0745
GUNN0746
GUNN0747
GUNN0748
GUNN0749
GUNN0750
GUNN0751
GUNN0752 THETA, VIS(COSI)
GUNN0753 TIMINSQ, TIMINSQ)
GUNN0754 UZERO, UZERO)
GUNN0755 USQ, USQ)
GUNN0756 ZMASS, X1, X1)

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GUNN0709 T, TMAX, TSIGSQ, TNEXT)
GUNN0710 I, TOVREL, THETA, WALL,
GUNN0711 ZMASS, ZMEMP, PROJ, XSTOP
GUNN0712 J, PROJ, JPROJQ2, JMIN, JMAX, J,
GUNN0713 K, L, MACHSQ, NDAT, E2,
GUNN0714 N, NMHAF, NPLUS1,
GUNN0715 P, PO, TO, AMOL, DUMVAR,
GUNN0716 CP(30), CV(30),
GUNN0717 C(200), PQ2(200), DS(200),
GUNN0718 GAMMA(30),
GUNN0719 MACHSQ(200), MEQST(30),
GUNN0720 ROZRO(30),
GUNN0721 THETA(200), UZERO(30),
GUNN0722 X(201, 2), X1(200),
GUNN0723 DUMVAR(500, 5)
GUNN0724 DTLAST, DLAST1)
GUNN0725 ESUM, EKSUM,
GUNN0726 HYDRD2, HYDRD3, OUTOTL1)
GUNN0727 SIGMA, SIGMIN, TMAX1)
GUNN0728 TPRINT, TNEXT)
GUNN0729 XGRID, XMIN, XMAX, EMPROJ)
GUNN0730 JPROJ, J,
GUNN0731 JMIN, JMAX, J,
GUNN0732 JPROJQ2)
GUNN0733 JMIN1)
GUNN0734 NUMBER, NTV)
GUNN0735 NPLUS1, NPLHAF, NN, NPL3HF)
GUNN0736
GUNN0737
GUNN0738 R,
GUNN0739 HALFRQ,
GUNN0740 ROZREI,
GUNN0741 INTERJ,
GUNN0742 TOVREI)
GUNN0743
GUNN0744
GUNN0745
GUNN0746
GUNN0747
GUNN0748
GUNN0749
GUNN0750
GUNN0751
GUNN0752
GUNN0753
GUNN0754
GUNN0755
GUNN0756

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UUU


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CALL      ZEROB(E,200,2)
CALL      ZEROB(AFEA,200,2)
CALL      ZEROB(Q,200,2)
CALL      ZEROB(U,201,2)
CALL      ZEROB(V,200,2)
CALL      ZEROB(P,200,2)
CALL      ZEROB(X,201,2)
RETURN
END
C
SUBROUTINE IERO(I1,I2,I3,I4,I5,I6,I7,I8)
ZEROS INTEGERS
I1=0
I2=0
I3=0
I4=0
I5=0
I6=0
I7=0
I8=0
RETURN
END
C
SUBROUTINE ZERO(Z1,Z2,Z3,Z4,Z5,Z6,Z7,Z8)
ZEROS NON-INTEGERS
Z1=0.
Z2=0.
Z3=0.
Z4=0.
Z5=0.
Z6=0.
Z7=0.
Z8=0.
RETURN
END
C
SUBROUTINE ZEROA(IZA,ZA1,ZA2,ZA3,ZA4,ZA5)
ZEROS VECTORS
DIMENSION ZA1(300),ZA2(300),ZA3(300),ZA4(300),ZA5(300)
DO 1 I,ZZ=1, IZA
  ZA1(I,ZZ)=0.
  ZA2(I,ZZ)=0.
  ZA3(I,ZZ)=0.
  ZA4(I,ZZ)=0.
  ZA5(I,ZZ)=0.
  CCNTINUE
1
RETURN
END
C
SUBROUTINE ZEROB(ZAB,IZA,JZB)
ZEROS ARRAYS
DIMENSION ZAB (300,10)

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GUNNO757
GUNNO758
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GUNNO797
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GUNNO799
GUNNO800
GUNNO801
GUNNO802
GUNNO803
GUNNO804

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DO 2 JZ=1, IZA
DO 1 JZZ=1, JZB
1 ZAB(IJZZ, JZZ)=0.
2 CONTINUE
RETURN
END

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SLBROUTINE STORIN (ISTORM, STORM)

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```

CCOMMON PCON3, SLOPE, RADIA3, CALPGM, TBRND, GMSRDR, GASPRS, IHEL
CCOMMON AREA1, AREA2, DTSQ, AREC3, CQSQ, CMAXR, CCO, CSQMA, C, CP, CMU, CPDE,
1 DPTMU, CCL, DQZDS, GAMMA, HALFM, PCON2, PPLUSQ, P, PI, Q, RQZRC, SHPR,
2 QWRONG, EL, FORCE, EZERO, HALFM, PCON2, PPLUSQ, P, PI, Q, RQZRC, SHPR,
3 EWRONG, EL, FORCE, EZERO, HALFM, PCON2, PPLUSQ, P, PI, Q, RQZRC, SHPR,
4 SIGMAX, SIGMIN, SKIN, TMAX1, TMAX2, TVDT1, TVDT2, TMAX, TSI, TSSQ, TNEXT,
5 TPRINT, TVNEXT, TMIN, TSCOS, X, XI, XGRID, XMIN, XMAX, ZMAX, EMPROJ, XSTOP,
6 VZERO, V, VOLUME, VISCOS, X, XI, XGRID, XMIN, XMAX, ZMAX, EMPROJ, XSTOP,
7 VZERO, V, VOLUME, VISCOS, X, XI, XGRID, XMIN, XMAX, ZMAX, EMPROJ, XSTOP,
CCOMMON IMAX, INU, I, INTERJ, INDEXT, ILIMIT, JPROJ1, JPROJ2, JMIN, JMAX, J,
1 JPLAKE, JMHFE, JLAST, JLAST, JLAST, JLAST, JLAST, JLAST, JLAST, JLAST, JLAST,
2 NCALF3, NUMB, NLF, NP, IQUIT, NQZRC, NQZRC, NQZRC, NQZRC, NQZRC, NQZRC, NQZRC,
3 NPLHAF, NUMB, NLF, NP, IQUIT, NQZRC, NQZRC, NQZRC, NQZRC, NQZRC, NQZRC, NQZRC,
DIMENSION AREA(200, 2), CQSQ(400), DELX(30), CMAXR(30), CQSQ(30), DQZ(200), DS(200),
1 DTMIN(30), DLAMD(200), DTSQ(200), DTSQ(200), DTSQ(200), DTSQ(200), DTSQ(200), DTSQ(200),
2 EZERO(30), E(200, 2), EINT(30), EMIN(30), FORCE(200), GAMMA(30),
3 HALFM(200), HALFRO(30), HYDRA(200), INTERJ(30), P(200, 2), Q(200, 2), RQZRC(30),
4 NZONES(30), OUTBDY(30), PPLUSQ(200), T(200, 2), T(200, 2), T(200, 2), T(200, 2),
5 SKIN(200), TSI(200), TVDT1(30), TVDT2(30), TVDT1(30), TVDT2(30), TVDT1(30), TVDT2(30),
6 T(200, 2), USQ(200), VZ(200, 30), V(200, 2), DUNVAR(500, 5)
7 ZMAX(200), Z(200), Z(200), Z(200), Z(200), Z(200), Z(200), Z(200), Z(200), Z(200),
DIMENSION ICN(100), STORM(100)
JPROJ=0
ICUJ=0
PVMWANT=0.
PVSLEPE=0.
PRESGCG=0.
PVERR=0.
XPV2=0.
XPV1=0.
1) = IMAX
2) = NDATE1
3) = NDATE2
4) = NDATE3
5) = NUMBER
6) = NCBEKE
7) = INU
8) = JPROJ
9) = IHEL
10) = IDUM

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GUNN0805
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GUNN0807
GUNN0808
GUNN0809
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GUNN0848
GUNN0849
GUNN0850
GUNN0851
GUNN0852

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DO 1 IN=1, I MAX
  IN10=IN+10
  IN20=IN+20
  IN30=IN+30
  IN40=IN+40
  IN50=IN+50
  IN60=IN+60
  I STORM(IN10)= NEQSI(IN)
  I STORM(IN20)= NZONES(IN)
  I STORM(IN)= OUTBDY(IN)
  STORM(IN10)= GAMMA(IN)
  STORM(IN20)= CQSQX4(IN)
  STORM(IN30)= UZERO(IN)
  STORM(IN40)= PO (IN)
  STORM(IN50)= TO (IN)
  STORM(IN60)= AMOL(IN)
1 CONTINUE
  STORM(71)= AREA1
  STORM(72)= AREA2
  STORM(73)= AREA3
  STORM(74)= PCON1
  STORM(75)= PCON2
  STORM(76)= SHPR
  STORM(77)= ENPROJ
  STORM(78)= OUTDI1
  STORM(79)= TMAX1
  STORM(80)= OUTDI2
  STORM(81)= TMAX2
  STORM(82)= XSTOP
  STORM(83)= PCON3
  STORM(84)= SLOPE
  STORM(85)= RADIUS
  STORM(86)= CALPGM
  STORM(67)= TURND
  STORM(88)= GSPDR
  STORM(89)= GASPRS
  STORM(90)= R
  STORM(91)= RPIST
  STORM(92)= PVWAST
  STORM(93)= PVSLEPE
  STORM(94)= XPV1
  STORM(95)= XPV2
  STORM(96)= PVERR
  STORM(97)= PRESCG
RETURN
END
SUBROUTINE STORE (ISTORM, STORM)
C STORAGE ROUTINE

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GUNNO853
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GUNNO866
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GUNNO895
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GUNNO899
GUNNO900

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[illegible]

U


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3  HALFM(200), HALFR(30), HYDRAD(200), INTERJ(31), MACHSQ(200), NEQST(30),
4  NZONES(30), OUTBDY(30), PPLSQ(200), P(200,2), Q(200,2), ROZERO(30),
5  SXIN(200), TSGSQ(200), TMINSQ(2), TQVREL(30), TQVREL(200), UZERO(30),
6  U(200,2), USQ(201), VZERO(30), V(200,2), VISCOS(200), X(201,2), X1(200),
7  X2(200,2), X3(200), X4(200), X5(200), X6(200), X7(200), X8(200), X9(200),
8  X10(200), X11(200), X12(200), X13(200), X14(200), X15(200), X16(200),
9  X17(200), X18(200), X19(200), X20(200), X21(200), X22(200), X23(200),
10 X24(200), X25(200), X26(200), X27(200), X28(200), X29(200), X30(200),
11 X31(200), X32(200), X33(200), X34(200), X35(200), X36(200), X37(200),
12 X38(200), X39(200), X40(200), X41(200), X42(200), X43(200), X44(200),
13 X45(200), X46(200), X47(200), X48(200), X49(200), X50(200), X51(200),
14 X52(200), X53(200), X54(200), X55(200), X56(200), X57(200), X58(200),
15 X59(200), X60(200), X61(200), X62(200), X63(200), X64(200), X65(200),
16 X66(200), X67(200), X68(200), X69(200), X70(200), X71(200), X72(200),
17 X73(200), X74(200), X75(200), X76(200), X77(200), X78(200), X79(200),
18 X80(200), X81(200), X82(200), X83(200), X84(200), X85(200), X86(200),
19 X87(200), X88(200), X89(200), X90(200), X91(200), X92(200), X93(200),
20 X94(200), X95(200), X96(200), X97(200), X98(200), X99(200), X100(200),
21 X101(200), X102(200), X103(200), X104(200), X105(200), X106(200),
22 X107(200), X108(200), X109(200), X110(200), X111(200), X112(200),
23 X113(200), X114(200), X115(200), X116(200), X117(200), X118(200),
24 X119(200), X120(200), X121(200), X122(200), X123(200), X124(200),
25 X125(200), X126(200), X127(200), X128(200), X129(200), X130(200),
26 X131(200), X132(200), X133(200), X134(200), X135(200), X136(200),
27 X137(200), X138(200), X139(200), X140(200), X141(200), X142(200),
28 X143(200), X144(200), X145(200), X146(200), X147(200), X148(200),
29 X149(200), X150(200), X151(200), X152(200), X153(200), X154(200),
30 X155(200), X156(200), X157(200), X158(200), X159(200), X160(200),
31 X161(200), X162(200), X163(200), X164(200), X165(200), X166(200),
32 X167(200), X168(200), X169(200), X170(200), X171(200), X172(200),
33 X173(200), X174(200), X175(200), X176(200), X177(200), X178(200),
34 X179(200), X180(200), X181(200), X182(200), X183(200), X184(200),
35 X185(200), X186(200), X187(200), X188(200), X189(200), X190(200),
36 X191(200), X192(200), X193(200), X194(200), X195(200), X196(200),
37 X197(200), X198(200), X199(200), X200(200), X201(200), X202(200),
38 X203(200), X204(200), X205(200), X206(200), X207(200), X208(200),
39 X209(200), X210(200), X211(200), X212(200), X213(200), X214(200),
40 X215(200), X216(200), X217(200), X218(200), X219(200), X220(200),
41 X221(200), X222(200), X223(200), X224(200), X225(200), X226(200),
42 X227(200), X228(200), X229(200), X230(200), X231(200), X232(200),
43 X233(200), X234(200), X235(200), X236(200), X237(200), X238(200),
44 X239(200), X240(200), X241(200), X242(200), X243(200), X244(200),
45 X245(200), X246(200), X247(200), X248(200), X249(200), X250(200),
46 X251(200), X252(200), X253(200), X254(200), X255(200), X256(200),
47 X257(200), X258(200), X259(200), X260(200), X261(200), X262(200),
48 X263(200), X264(200), X265(200), X266(200), X267(200), X268(200),
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213 X1253(200), X1254(200), X
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130 IF(INDEX.EQ.3)CALL EQST3
CONTINUE
135 JMNHAF=1,JLAST1
135 PPLUSQ(JMNHAF)=P(JMNHAF,N)
150 DK=1,2
DK1=2,0.
EKSUM=0.
EKSUM=0.
ETOT=0.
USQ(1)=U(1,N)**2
DO 165 I=1,IMAX
EINT(I)=0.
EKN(I)=0.
JMIN=INTERJ(I)
JMAX=INTERJ(I,1)-1
DO 160 J=JMIN,JMAX
JPLHAF=J
USQ(J+1)=U(J+1,N)**2
EINT(J+1)=E(JPLHAF,N)/HALFRO(I)*HALFM(JPLHAF)*DK
160 EKN(I)=(USQ(J)+USQ(J+1))*HALFM(JPLHAF)*DK+EKN(I)
EKSUM=EKSUM+EINT(I)
165 ETOT=ETOT+EKSUM
EKSUM=EKSUM+EKN(I)
EKSUM=EKSUM+EKN(I)
EKSUM=EKSUM+EKSUM
EKSUM=ETOT
ETENTH=1*ETOT
XGRID=.125*(X(JMAX,N)-X(1,N))
175 XMIN=X(1,N)-XGRID
XMAX=X(JMAX,N)+XGRID
180 CALL OUTPUT
RETURN
END
SUBROUTINE DYNMEQ
CALCULATES MASS POINT VELOCITY AND ZONE SPECIFIC VOLUME AND
COMMON PCON3,SLOPE,RADIUS,CALPGM,TBURND,GMSFDR,GASPRS,IHEL
COMMON AREAL,AREA2,AREA3,AREA,CQSQX4,CMAXR,CSQ,CSQMAX,CP,CV,DLAMAX
1 DPCM,DUOT,DIAMDA,DIQ,DITLAST,ESUM,EKSUM,EINT,EKIN,E,ETOT,ETENTH,
2 DTMCN,Q1,DQ2,DQ3,EZERQ,EINSUM,HALFM,HALFRO,HYDRD1,HYDRD2,HYDRD3,HYDRAD,
3 EWRONG,EL,FORCE,GAMMA,HALFRO,PCON2,PPLUSQ,P1,Q,ROZERC,SHPR,
4 QUTBDY,QUTDT,QUTDI,QUTDI2,QUTDI3,QUTDI4,QUTDI5,QUTDI6,QUTDI7,
5 SIGMAX,SIGMIN,SIGIN,SIGOUT,SIGOUT2,SIGOUT3,SIGOUT4,SIGOUT5,
6 PRINI,TVOLUME,VISCOS,X,XI,XGRID,XMIN,XMAX,ZMAX,EMPROJ,XSTOP,
7 VZERON,VOLUME,VISCOS,X,XI,XGRID,XMIN,XMAX,ZMAX,EMPROJ,XSTOP,
8 COMMON IMAX,J,JLAST1,JMIN1,JMIN2,JMIN3,JMIN4,JMIN5,JMIN6,JMIN7,
1 JPLHAF,JMNHAF,JLAST1,JMIN1,JMAX1,K,L,MACHSQ,NDAF,NPLUS1,
2 NDATE3,NUMBER,NV,NCHEKE,NEQS,NZONES,NCYCLES,NMNMHAF,NPLUS1,
3 NPLHAF,NN,NPL3HF,NP,IQUIT,JPROJ,JSTOP,EMPIST,PO,TO,AMOL,DUMVAR
GUNN1045
GUNN1046
GUNN1047
GUNN1048
GUNN1049
GUNN1050
GUNN1051
GUNN1052
GUNN1053
GUNN1054
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GUNN1088
GUNN1089
GUNN1090
GUNN1091
GUNN1092

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CC


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DIMENSION AREA(200,2), CQSQX4(30), CMAXR(30), CSQ(200), CP(30), CV(30), GUNN1093
1DTMIN(3), DELAMDA(20), DTSQ(200), DQ1(200), DQ2(200), DS(200), GUNN1094
2VZERO(30), E(200,2), EINT(30), EKINT(30), FORCE(200), GAMMA(30), GUNN1095
3HALFM(200), HALFBY(30), HYDRA(200), INTERJ(31), MACSQ(200), NEQST(30), GUNN1096
4NZNONES(30), OUTBDY(30), PPLUSQ(200), PL(200,2), Q(200,2), ROZERO(30), GUNN1097
5XIN(200), TSIGSQ(200), TMINSQ(21), TVREI(30), TETA(200), UZERO(30), GUNN1098
6U(200,2), USQ(201), VZERO(30), V(200,2), VISCS(200), X(201,2), X1(200), GUNN1099
7ZMASS(200), PO(30), TO(30), AMOL(30), DUMVAR(500,5)
      I=1
      CCNTINUE
      DLAMAX=0.
      SIGMAX=0.
      T=T+DTMIN(NPLHAF)
      NCYCLE=NCYCLE+1
      DO 245 I=1,IMAX
      DO 245 I=1,IMAX
      NZN=NZNONES(I+1)
      CMAXR(I)=0.
      CSCMAX=0.
      JMIN=INTERJ(I)+1
      JMAX=INTERJ(I+1)
      DO 230 J=JMIN, JMAX
      JPLHAF=J
      JMNHAF=J-1
      IF(JLAST-J) 155,155,1700
      DUDT=PPLUSQ(JMNHAF)*AREA(JLAST,N)/HALFM(JMNHAF)
      IF(JPROJ.EQ.300.AND.E(JMNHAF,N).NE.0.0) GC TO 195
      GO TO 901
      IF(JPROJ.EQ.300) GO TO 1755
      IF(J.EQ.INTERJ(6)) GO TO 901
      IF(J.GT.INTERJ(6)) GO TO 902
      GO TO 1755
      IF(PPLUSQ(JMNHAF)-SHPR) 902,903,903
      U(J,NPLHAF)=0.0
      GC TO 196
      JPROJ=500
      DTSQ(200)=T
      IF(J.EQ.JMAX.AND.NZN.EQ.1) GO TO 876
      IF(J.EQ.JMAX.AND.NZN.GT.1) GO TO 800
      DUDT=(PPLUSQ(JMNHAF)-PPLUSQ(JPLHAF))*AREA(J,N)/(HALFM(JMNHAF)+
      1HALFM(JPLHAF))
      GC TO 195
      800 IF(J.EQ.INTERJ(6)) GO TO 863
      DUDT=-((1.5*(PPLUSQ(JPLHAF)-PPLUSQ(JMNHAF))-(PPLUSQ(JPLHAF+1)-
      1PPLUSQ(JMNHAF-1))/6.)*AREA(J,N)/(HALFM(JMNHAF)+HALFM(JPLHAF))
      GC TO 195
      863 DUDT=-((1.5*(PPLUSQ(JPLHAF)-PPLUSQ(JMNHAF))-(PPLUSQ(JPLHAF+1)-
      1PPLUSQ(JMNHAF-1))/3.+2.*PPLUSQ(JMNHAF-1)/3.))
      11/6.)*AREA(J,N)/(HALFM(JMNHAF)+HALFM(JPLHAF))

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154 IF (T-GE.(DTSQ(200)+DTSQ(199))) GO TO 194
    DUDT=DUDT*(T-DTSQ(200))/DTSQ(199)
    CONTINUE
155 GO TO 155
1876 A=2.*HALFM(JMNHAF)+HALFM(JPLHAF)
    B=HALFM(JMNHAF)+PPPLUSQ(JPLHAF)
    DUDT=((2.*A**2*PPPLUSQ(JLNMHAF)
1-1(2.*A-B)*(A+B)*PPPLUSQ(JLNMHAF)
2+(A-B)*B*PPPLUSQ(JMNHAF-1))/(A*(A+B)*B)*AREA(J,N)
155 U(J,NPLHAF)=U(J,NMNHAF)+DTMIN(NN)*DUDT
156 X(J,NPLUS1)=X(J,N)+DTMIN(NPLHAF)*U(J,NPLHAF)
    CALL ARCOMP
    CALL VCQMP
    V(JMNHAF,NPLUS1)=HALFRO(I)/HALFM(JMNHAF)*VOLUME
200 IF (U(J,NPLHAF)-U(J-1,NPLHAF)) 205,225,225
205 Q(JMNHAF,NPLHAF)=CSQX4(I)*HALFRO(I)*(U(J,NPLHAF)-U(J-1,NPLHAF))
1*Q*(V(JMNHAF,NPLUS1)+V(JMNHAF,N))
    GO TO 230
225 Q(JMNHAF,NPLHAF)=0.
230 CONTINUE
    INDEX=NEQST(I)
    IF (INDEX.EQ.1) CALL ECST1
    IF (INDEX.EQ.2) CALL ECST2
    IF (INDEX.EQ.3) CALL ECST3
53 DO 240 J=JMIN,JMAX
    JMNHAF=J-1
    IF (JPROJ.LT.300.AND.J.GT.INTERJ(6)) GO TO 24
    TSIGSQ(JMNHAF)=CSQ(JMNHAF)/(X(J,NPLUS1)-X(J-1,NPLUS1))*2
24 CONTINUE
    PPLUSQ(JMNHAF)=P(JMNHAF,NPLUS1)+Q(JMNHAF,NPLHAF)
    DLAMDA(JMNHAF)=CSQX4(I)/2.*(V(JMNHAF,N
1(V(JMNHAF,N)+V(JMNHAF,NPLUS1))
    CFANGED TO MAX1 JANUARY 1967 DKS
    DLAMAX=MAX1(DLAMDA(JMNHAF),DLAMAX)
    SIGMAX=MAX1(TSIGSQ(JMNHAF),SIGMAX)
    CSQMAX=MAX1(CSQMAX,CSQ(JMNHAF))
    IF (TSIGSQ(JMNHAF).NE.0.0) GO TO 240
    DTSQ(JMNHAF)=0.0
    GO TO 245
240 DTSQ(JMNHAF)=111111/TSIGSQ(JMNHAF)
245 CMXR(I)=SORT(CSQMAX)
340 CONTINUE
246 RETURN
END
C
SUBROUTINE ARCOMP
    DETERMINES ZONE CROSS SECTIONAL AREA
    COMMON PCOM3,SLOPE,RADIUS,CALPGM,TBURND,GMSFDR,GASPRS,IHEL
    COMMON ARE1,AREA2,AREA3,AREA,CQSQX4,CMAXR,CSQ,CSQMAX,CP,CV,DLAMAX
    GUNN1141
    GUNN1142
    GUNN1143
    GUNN1144
    GUNN1145
    GUNN1146
    GUNN1147
    GUNN1148
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    GUNN1172
    GUNN1173
    GUNN1174
    GUNN1175
    GUNN1176
    GUNN1177
    GUNN1178
    GUNN1179
    GUNN1180
    GUNN1181
    GUNN1182
    GUNN1183
    GUNN1184
    GUNN1185
    GUNN1186
    GUNN1187
    GUNN1188

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2 EZERO(30), F(200,2), EINT(30), EKIN(30), FORCE(200), GAMMA(30),
3 ALRM(200), HALFRO(30), HYDRAD(200), INTERJ(31), MACHSQ(200), NEQST(30),
4 NZONES(30), OUTBDY(30), PPLUSQ(200), P(200,2), Q(200,2), ROZERO(30),
5 SKIN(200), TSIGSQ(200), TMSQ(200), TVREL(30), THETA(200), UZERO(30),
6 U(201,2), USQ(201), VZERO(30), V(200,2), VISCCS(200), X(201,2), X1(200),
7 MASS(200), PD(30), TD(30), AMOL(30), DUMVAR(500,5)
8 XPI1=0.
9 XPI2=0.
10 PVKRG=0.
11 PRESRG=0.
12 IF(X(J,NPLUS1)-PCON1) 3,3,4
13 VOLUME=(X(J,NPLUS1)-X(J-1,NPLUS1))*AREA1
14 GO TO 17
15 IF(X(J,NPLUS1)-PCON2) 5,5,8
16 IF(X(J-1,NPLUS1)-PCON1) 6,7
17 VOLUME=(X(J,NPLUS1)-PCON1)*AREA2+(PCON1-X(J-1,NPLUS1))*AREA1
18 GO TO 17
19 VOLUME=(X(J,NPLUS1)-X(J-1,NPLUS1))*AREA2
20 GO TO 17
21 IF(X(J,NPLUS1)-PCON3) 9,9,12
22 IF(X(J-1,NPLUS1)-PCON2) 10,11,11
23 VOLUME=(X(J,NPLUS1)-X(J-1,NPLUS1))*AREA2
24 GO TO 17
25 VOLUME=(X(J,NPLUS1)-X(J-1,NPLUS1))*AREA2
26 GO TO 17
27 IF(X(J-1,NPLUS1)-PCON3) 14,13,13
28 VOLUME=(X(J,NPLUS1)-X(J-1,NPLUS1))*AREA3
29 GO TO 17
30 IF(X(J-1,NPLUS1)-PCON2) 16,15,15
31 VOLUME=(X(J,NPLUS1)-X(J-1,NPLUS1))*AREA3
32 GO TO 17
33 VOLUME=(X(J,NPLUS1)-X(J-1,NPLUS1))*AREA3
34 RETURN
35 END
36 SUBROUTINE EQST1
37 CALCULATE PRESSURE AND ENERGY FOR IDEAL GAS ZONES
38 COMMON PCON3, SLOPE, RAD, CALPGM, TOURND, GAS, QRS, IHEL, CV, DLAMAX,
39 COMMON AREA1, AREA2, AREA3, AREA4, CQSQX4, CMA, XRS, CSQ, CMA, X, CMU, DPDE,
40 1, DTMIN, DUDT, DLAMDA, DTSC, DLAST, DLAST, DNZONE, E, ETOI, TENTH,
41 2, PCDU, DQ1, Q2, DS, EZERO, EINSUM, ESUM, EKSUM, E, ETOI, TENTH,
42 3, OUTBDY, EL, FORCE, GAMMA, HALFRO, HYDRD1, HYDRD2, HYDRD3, HYDRAD,
43 4, OUTBDY, OUTDT1, PCON1, PCON2, PPLUSQ, P, PI, Q, ROZERO, SHPR,
44 5, SIGMAX, SIGMIN, SKIN, TMAX2, TVD1, TVD2, TMAX, TSIGSQ, TNEXT,
45 6, TPRINT, TVNEL, TMIN, SQ, TVFREQ, UZERO, U, USQ, TBA, TOVREL, TPROJ, TALL,
46 7, VZED, V, VOLUME, VISQ, X, X1, XGRI, YMIN, XMAX, ZMASS, ZTALL,
47 8, VZED, V, VOLUME, VISQ, X, X1, XGRI, YMIN, XMAX, ZMASS, ZTALL,
49 COMMON IMAX, INU, I, INTERJ, INDEX, ILIMIT, JPROJ, JMAX, J,
1 JPLTHAF, JMNHAF, JLAST, JLAST, JMINI, JMAXI, K, L, MACHSQ, NDATEI, NDATE2,
2 NCDATE3, NUMBER, NTV, NCHEKE, NEQST, NZONES, NCYCLE, N, NMNINHAF, NPLUS1,

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C


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BNPLHAF,N,N,NPL3HF,NP,IQUIT,JPROJ,JSTOP,R,EMPIST,PO,TO,AMOL,DUMVAR
DIMENSI(3),DLAMDA(200,2),CQSQX4(30),CHAXP(30),CQ(200),CP(30),CV(30),
DIDDMIN(3),DLAMDA(200,2),DTSQ(200),DELX(30),DGL(200),DQ2(200),D3(200),
DZER(30),E(200,2),EINT(30),EKN(30),FORCE(200),GAMMA(30),
HALFRQ(200),HALFRQ(30),HYRAD(200),INTERJ(31),MACHSQ(200),NEOST(30),
NPLHAFM(30),OUTBDY(30),PPLUSQ(200,1),P(200,2),Q(200,2),ROZERO(30),
55KINZONES(30),OUTBDY(30),TMSQS(2),TOYREL(30),THETA(200),UZERO(30),
GUNN1289
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GUNN1333
BNPLHAF,N,N,NPL3HF,NP,IQUIT,JPROJ,JSTOP,R,EMPIST,PO,TO,AMOL,DUMVAR
DIMENSI(3),DLAMDA(200,2),CQSQX4(30),CHAXP(30),CQ(200),CP(30),CV(30),
DIDDMIN(3),DLAMDA(200,2),DTSQ(200),DELX(30),DGL(200),DQ2(200),D3(200),
DZER(30),E(200,2),EINT(30),EKN(30),FORCE(200),GAMMA(30),
HALFRQ(200),HALFRQ(30),HYRAD(200),INTERJ(31),MACHSQ(200),NEOST(30),
NPLHAFM(30),OUTBDY(30),PPLUSQ(200,1),P(200,2),Q(200,2),ROZERO(30),
55KINZONES(30),OUTBDY(30),TMSQS(2),TOYREL(30),THETA(200),UZERO(30),
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U


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IBURND=0
TOLD=0.
INTERJ(30)=2
ZMAS(200)=2
GASPRS=GASPRS/14.5
PVOL=GMSPDR/1000.
GVOL=PCONI*AREAL*.001-PVOL
PMOL=GMSPDR/25.
PMOLES=GMSPDR/25.
PRESUR=(GMOL*PMOLES)*24.61/(GVOL+PVOL)*1.0138
35 GAMMA(I)=(GMOL*PMOLES*1.667+PMOLES*1.23)/(GMOL*PMOLES)
WGT MOL=(GMOL*PMOLES*4.0026+PMOLES*25.0)/(GMOL*PMOLES)
GO TO 50
40 GAMMA(I)=(GMOL*PMOLES*1.4+PMOLES*1.23)/(GMOL*PMOLES)
WGT MOL=(GMOL*PMOLES*2.0+PMOLES*25.0)/(GMOL*PMOLES)
50 SPCVOL=83.17*300.0/(PRESUR*WGT MOL)
RZERO(I)=SPCVOL/RZERO(I)
EZERO(I)=PRESUR/VZERO(I)/(GAMMA(I)-1.0)
JMINI=JMIN-1
JMAXI=JMAX-1
DO 20 J=JMINI,JMAXI
E(J,N)=EZERO(I)
20 EPEAK=CALPGM*41.84*RZERO(I)*PMOLES*25.0/(PMOLES*25.0+GMOL*2.0)
HALFRO(I)=RZERO(I)/2.
DC 30 J=JMIN,JMAX
VOLUME=(X(J,N)-X(J-1,N))*AREAL
30 HALFRO(I)=HALFRO(I)/V(J-1,N)*VOLUME
JMINI=JMIN-1
JMAXI=JMAX-1
IF(TBURND)4,4,7
4 IF(TBURND.EQ.0.0) GO TO 6
STATEMENT IF(TBURND.EQ.0.0) GO TO 6 WAS INSERTED DURING CON-
VERSION TO THE G.E. 635
5 DEL=EPEAK*(T-TOLD)/TBURND
TOLD=T
GO TO 7
6 DEL=0.
7 DO 10 JMNHAF=JMINI,JMAXI
E1=E(JMNHAF,N)-(P(JMNHAF,N)+Q(JMNHAF,NPLHAF))* (V(JMNHAF,NPLUS1)-
1V(JMNHAF,N))+DEL
P1=(GAMMA(I)-1.0)*E1/V(JMNHAF,NPLUS1)
E(JMNHAF,NPLUS1)=E1-.5*(P1-P(JMNHAF,N))* (V(JMNHAF,NPLUS1)-
1V(JMNHAF,N))

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GUNN1380

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P(JMNHAF,NPLUS1)=(GAMMA(I)-1.)*E(JMNHAF,NPLUS1)/V(JMNHAF,NPLUS1)
10 CSQ(JMNHAF)=GAMMA(I)*(GAMMA(I)-1.)*E(JMNHAF,NPLUS1)/ROZERO(I)
RETURN
END
SUBROUTINE EQST3
CALCULATE PRESSURE AND ENERGY FOR SOLID ZONES
COMMON PCOM3,SLOPE,RADIUS,CALPGM,TBYRND,GMSDDR,GASPRS,IHEL
COMMON AREA3,AREA2,AREA1,CQSQX,CMAXR,CQSQX,CQSQX,CP,CMV,DLAMAX
1,DTMIN,DUD,DLAMDA,DTSQ,TLAST,DLASL,DLJLST,CMAXR,CQSQX,CP,CMV,DLAMAX
2PDMU,DQ1,DQ2,DS,EMERO,EINUM,ESUM,EKSUM,EINT,EKIN,HYDRD1,HYDRD2,HYDRD3,HYDRD,
3EKRNG,EL,FORCE,GAMMA,HALFM,HALFRO,HYDRQ,P,P1,Q,ROZ,ROZD3,HPR,
4OUTBDY,OUTOT1,OUTOT2,PCON1,PCON2,PPLUSQ,P,P1,Q,ROZ,ROZD3,HPR,
5SIGMAX,SIGMIN,SKINX,TMAX1,TMAX2,TVD1,TVD2,TMAX,TSIGSQ,TNEXT,
6PRINT,VOLUME,TMINSQ,TVFREQ,UZERU,USQ,TBAT,TOVRE1,THETA,TWALL,
7VZRO,VVOL,X,X1,XGRD,XMIN,XMAX,XMAS,EMPROJ,XSTOP,
COMMON I,MX,INU,I,INTERJ,INDEX,ILIMIT,JPROJ2,JMIN,JMAX,J,
1JPMHAF,JMNHAF,JJ,AST,JLAST,JMINI,JMAXI,K,L,JACHSQ,NDA
2NDAT3,NUMBER,NIV,NCKE,NEST,NZONES,NCYCL,N,NMNHAF,NPLUS1,
3NPLHAF,NN,NPL3HF,NP,IQUIT,JPROJ,JSTOP,R,EMP,ST,PO,TO,AMOL,DUMVAR
4DIMENSION AREA(200),CQSQ(200),CMAXR(30),DSQ(200),CP(30),CV(30),
1DTMIN(30),DLAMDA(200),DTSQ(200),DELX(30),DQ1(200),DQ2(200),DS(200),
2EZERO(30),E(200,2),EINT(30),EKIN(30),FORCE(200),GAMMA(30),
3HALFM(200),HALFRDY(30),HYDRQ(200),INTERJ(31),MACHSQ(200),NEQT(30),
4NZONES(30),OUTBDY(30),PPLUSQ(200),P(200,2),Q(200,2),ROZD3(30),
5SKIN(200),TSIGSQ(200),TMINSQ(2),TOVRE1(30),THETA(30),UZERO(30),
6U(200,2),USQ(200),VZRO(30),V(200,2),VISCOS(200),X(201,2),X1(200),
7ZMAS(200),P(30),AMOL(30),DUMVAR(500,5)
JMINI=JMIN-1
JMAXI=JMAX-1
DO 10 JMNHAF=JMINI,JMAXI
CMU=1./V(JMNHAF,NPLUS1)-1.
E1=E(JMNHAF,N)
1V(JMNHAF,N)
P(JMNHAF,N)+Q(JMNHAF,NPLHAF))*(V(JMNHAF,NPLUS1)-
1V(JMNHAF,N))
PDMU=21297.0*(DMU+1.0)**6-3041.4
P(JMNHAF,NPLUS1)=3042.4*(DMU+1.0)**7-3041.4
IF(P(JMNHAF,NPLUS1)>5000.0) 9,11,11
5 P(JMNHAF,NPLUS1)=3000.
11 E(JMNHAF,NPLUS1)=E1-.5*(P(JMNHAF,NPLUS1)-P(JMNHAF,N))*(V(JMNHAF,
1NPLUS1)-V(JMNHAF,N))
10 CSQ(JMNHAF)=DPMU/ROZERO(I)
RETURN
END
SUBROUTINE PVCHNG (PVW, ERR, VEL,PLOAD, GAS, AVEL, ALOAD, AGAS,NU)
DIMENSION GAS(30), AVEL(100), ALOAD(100), AGAS(100)
PVW=10
PVLO=10
20 N=1,NU
5000.
IF (AGAS(N).NE.GAS(3)) GO TO 20

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IF (ABS(AVEL(N)-PVW).LT.ERR) GO TO 30
IF (AVEL(N).GT.PVW.AND.AVEL(N).GT.PVHI) GO TO 20
IF (AVEL(N).LT.PVW.AND.AVEL(N).LT.PVLO) GO TO 20
IF (AVEL(N).LT.PVW) GO TO 40
HLOAD=ALOAD(N)
PVHI=AVEL(N)
GO TO 20
40 BALOAD=ALOAD(N)
PVLO=AVEL(N)
20 CONTINUE
IF(PVLG.EQ.10.0.OR.PVHI.EQ.5000.) GO TO 60
PLOAD=BALOAD*(PVW-PVLO)*(BALOAD-HLOAD)/(PVLO-PVHI)
GC TO 50
30 PLGAD=ALOAD(N)
GO TO 50
60 PLOAD=PLOAD+(PVW-VEL)*20.
50 GAS(1)=PLOAD
RETURN
END

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INPUT FORMAT

CARD 1 (413,F10.0)
 IDATA = 0, STANDARD 18 CARD INPUT
 = NAMELIST INPUT OF ALL VARIABLES ON CARDS
 IPRNTZ = 0, STANDARD RUN
 = 1, PRINT OUT INITIAL DATA ONLY
 INTRNSF = 0, USE DISK SCRATCH FILE AND PRINT OUT ONLY LAST PISTON ITERATION
 = 1, PRINT OUT ALL PISTON ITERATIONS (HYPERVELOCITY MODEL ONLY)
 IPUNCH = 0, NO PUNCHED OUTPUT
 = 1, PUNCHED OUTPUT OF MODEL BASE PRESSURE VS TIME
 DTSQ(199) FINITE BREAK VALVE OPENING TIME

CARD 2 (2013)
 IMAX = NUMBER OF REGIONS (UP TO SIX)
 NDATE1 = MONTH
 NDATE2 = DAY
 NDATE3 = YEAR
 NUMBER = RUN IDENTIFICATION NUMBER
 NCHEKE = 0, NO ENERGY CHECK
 = 1, ENERGY MONITORED AND PROBLEM STOPPED IF THE TOTAL ENERGY
 CHANGES BY MORE THAN 10%
 INU = 0, ALL ZONES HAVE ZERO INITIAL VELOCITY
 = 1, ALLOWS INITIAL VELOCITY FOR EACH ZONE TO BE READ
 JPROJ = MASS POINT NUMBER OF PROJECTILE

CARD 3 (2013)
 NEQST(I) = NUMBER OR INDEX OF EQUATION OF STATE USED IN REGION I

CARD 4 (2013)
 NZONES(I) = NUMBER OF ZONES IN REGION I

CARD 5 (7F10.0)
 OUTBDY(I) = DISTANCE IN CM TO OUTER INTERFACE OF REGION I

CARD 6 (7F10.0)
 GAMMA(I) = RATION OF SPECIFIC HEATS FOR REGION I

CARD 7 (7F10.0)
 CQSQX4(I) = CONSTANT USED IN ARTIFICIAL VISCOSITY COMPUTATION
 (GOOD VALUES ARE 4.0 FOR GAS REGION, 9.0 FOR SOLID REGION)

CARD 8 (7F10.0)
 AREA1 = AREA IN SQ CM OF FIRST CONSTANT AREA SECTION (PROGRAM ALLOWS UP TO
 THREE DIFFERENT CONSTANT AREA SECTIONS AND ONE TAPERED SECTION
 BETWEEN THE SECOND AND THIRD CONSTANT AREA SECTIONS)
 AREA2 = AREA IN SQ CM OF SECOND CONSTANT AREA SECTION
 AREA3 = AREA IN SQ CM OF THIRD CONSTANT AREA SECTION
 PCON1 = POSITION IN CM WHERE FIRST AREA CHANGE OCCURS
 SHPR = PROJECTILE RELEASE PRESSURE IN BARS
 EMPROJ = MASS OF PROJECTILE IN GRAMS

OUTDT1 = DELTA T FOR PRINTING UP TO TIME TMAX1
 TMAX1 = MILLISECS
 OUTDT2 = DELTA T FOR PRINTING UP TO TIME TMAX2
 TMAX2 = MILLISECS
 XSTOP = POSITION IN CM THAT WHEN THE INTERFACE JSTOP REACHES IT,
 THE PROBLEM IS TERMINATED

CARD 9 (7F10.0) REQUIRED ONLY IF INU = 1
 UZERO(1) = INITIAL VELOCITY FOR EACH ZONE

CARD 10 (7F10.0)
 PCON = POSITION IN CM WHERE THIRD AREA CHANGE OCCURS
 SLOPE = SLOPE OF CONSTANT TAPERED SECTION
 RADIUS = RADIUS IN CM OF THE CONSTANT AREA SECTION TO THE RIGHT
 OF THE TAPERED SECTION

CARD 11 (4F10.0I4)
 CALPGM = CALORIES PERGRAM OF POWDER
 TBURND = TIME TO BURN POWDER
 GMSPPDR = GRAMS OF POWDER
 GASPRS = INITIAL GAS PRESSURE IN POWDER REGION
 IHREL = 0 (NOT APPLICABLE TO GUN PROJECT)

CARD 12 (7F10.0)
 IPOX = 0 ALL PLOTS, ALL PRESSURE POINTS (PLOT ROUTINE MUST BE INCLUDED)
 = 1 ALL PLOTS, NO PRESSURE POINTS
 = 5 NO PLOTS, NO PRESSURE POINTS
 = 6 ONLY PRESSURE POINTS
 NPOX = NUMBER OF PRESSURE POINTS (UP TO FIVE)
 XPO(1) = X POSITION IN CM OF PRESSURE POINT 1

CARD 13 (7F10.0) HYPERVELOCITY MODEL LAUNCHER PARAMETERS, (NOT APPLICABLE TO GUN PROJECT)
 XPV1 = X POSITION IN CM OF FIRST MEASUREMENT POINT OF PISTON VELOCITY
 XPV2 = X POSITION IN CM OF SECOND MEASUREMENT POINT OF PISTON VELOCITY
 PVERR = PISTON VELOCITY ERROR IN FT PER SEC
 PVWANT = DESIRED PISTON VELOCITY IN FT PER SEC

CARD 14 (E10.0, 3F10.0)
 R = 8317E 08 GAS CONSTANT
 EMP1ST = MASS OF FIRST PISTON SECTION (HYPERVELOCITY MODEL LAUNCHER ONLY)
 FRAC = 1.0
 EMLEAD = MASS OF SECOND PISTON SECTION (HYPERVELOCITY MODEL LAUNCHER)

CARD 15 (7F10.0)
 PO(1) = INITIAL PRESSURE IN PSI IN REGION 1

CARD 16 (7F10.0)
 TO(1) = INITIAL TEMPERATURE IN DEGREES KELVIN IN REGION 1

CARD 17 (7F10.0)
AMOL(I) = MOLECULAR WEIGHT OF MATERIAL IN REGION I

CARD 18 (I3)
ILASTK = 0, STOP
 = 1, CONTINUE FOR NEW RUN

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